

Enhancing the fire-resistance performance of composite laminates via multi-scale hybridisation: A review

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Enhancing the fire-resistance performance of composite laminates via multi-scale hybridisation: A review

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Abstract

Fibre-reinforced composites laminates (FRCLs) are employed in various applications such as in marine, aerospace, automotive, and civil industries due to their lightweight nature, design tailorability, and superior specific mechanical properties. However, they possess extremely low flame resistance mainly due to the inherent flammability of the polymer matrix. Various treatments have been applied to improve the fire resistance of FRCLs. In particular, hybridisation (fibre hybridisation and polymer hybridisation) is an important technique which is becoming very popular to enhance the thermal performance and flame resistance of FRCLs. This article is a comprehensive review of the recent developments that broadly cover the improvements in fire resistance of composite laminates via multi-scale hybridisation; the characteristics of thermal decomposition of FRCLs have been presented to comprehend the need for flame retardancy. Approaches for improving the fire resistance of FRCLs and thermal stability, both in polymer and in fibre systems, are

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discussed. Enhancing the fire resistance has been significant through additives to the matrix, use of flame-retardant modified fibres at interfacial regions and by way of multi-layered hybrid laminates besides hybridization at fibre, yarn and layer level. Finally, a review is presented on the modelling of fire resistance of composite laminates by considering thermo-mechanical models for the prediction of decomposition and failure of laminates at elevated temperatures.

Keywords

Fire resistance, composite materials, flammability, thermal decomposition, hybridisation

Introduction

In the last few decades, applications of fibre-reinforced composites (FRCLs) have rapidly increased and are anticipated to continue to grow in the future. This owes to the exceptional performance of composite materials in numerous structural applications such as aircraft, spacecraft, automobiles, boats, wind turbines, and civil infrastructure.¹⁻⁴ Polymer composites have excellent mechanical competences such as design flexibility, thermal resistance and good strength to weight ratio making them ideal for structural applications like door panels, body and chassis of cars, fuselage and fuselage windows in the aerospace and automotive particularly in severe environment.⁵ In addition, composite materials are gradually replacing metals and ceramics due to their superior properties such as lower density and thermal expansion, high values of specific stiffness and strength, good fatigue durability, high resistance to corrosion, and excellent thermal insulation.⁶⁻⁸ Nevertheless, their sensitivity to impact loading, anisotropic properties, and poor flame resistance due to the intrinsic flammability of the polymer matrix have limited their use in applications where fire safety and high-impact damage tolerance properties are required.⁹⁻¹⁴ Damage to composite laminates in a fire will strongly affect their structural integrity and post-fire performance; leading to reduction in their mechanical performance.¹⁵⁻¹⁷ The physical properties of composite laminates such as reduced weight, elasticity, and thermal and electrical conductivity are the controlling factors for the selection of suitable reinforcements.^{18,19} Matrix material (polymer) determines properties such as the interactivity of additive materials with the matrix, binding property, appearance, acquiescence with ambient conditions, voltage and load transformation, and protection against impact.^{20,21} Most of the synthetic fibres (being used as reinforcements) such as carbon, glass, and Kevlar have higher melting points and they appear to be highly fire resistant.¹⁴ Conversely, polymer matrices illustrate inherent flammability with quite complicated degradation and combustion processes.^{22,23} Different types of thermosets and thermoplastics are decomposed at a higher temperature (generally 300 to 400°C) which leads to inferior mechanical performance (i.e. tensile, compressive, and shear strengths) and produces heat, toxic smoke, and soot particles causing acute or delayed health problems.^{24,25} The degradation of the structural properties (i.e. strengths of composites) happen due to the damage controlled mainly by the chemical processes during the thermal

decomposition of the polymer matrix. In order to reduce the fire risks and retain important characteristics such as thermal stability and mechanical performance, many techniques have been adopted by researchers to achieve flame retardant performance.^{26–28} The hybridisation (fibre and polymer hybridisation) process is one paramount and effective way to improve the thermal stability, fire resistance and mechanical performance of FRCL materials.

This article is a comprehensive review of the recent developments that broadly cover the improvements in thermal stability and fire resistance of composite laminates via multi-scale hybridisation. The response and susceptibility of composite laminates on exposure to fire has been illustrated. Approaches for improving the fire resistance of FRCLs, both in polymer and in fibre systems, have been discussed. Various flame-retardant (FR) strategies, their mechanisms, and the decomposition of FRCLs have also been discussed. Based on their flammability and the rate at which flammable and toxic gaseous elements are discharged, various test methods have been discussed to study the fire behaviour of composite laminates. This paper also presents an introduction to typical FR requirements and a brief view on the flame retardation of FRCLs. The prime focus of this study has been to present insightful literature on improving the flame resistance and thermal stability of composite materials via multi-scale hybridisation techniques. These approaches include polymer toughening methods and modification of reinforcements. Furthermore, an effort is made to review the modelling of fire resistance of composite laminates by considering the thermal-mechanical models to predict decomposition and failure of laminates at elevated temperatures.

Flammability of composite laminates

Most FRCLs are combined with matrix materials, which are combustible at various temperatures. These composites can easily burn often by producing smoke compared to metals. Moreover, fibre reinforcements – both organic (i.e. cotton, wool, and silk) and inorganic fibres (i.e. polypropylene, polyester, aramid, carbon, and E-glass) – can behave as fuel for the burning of composites.²⁹ Therefore, the high susceptibility of the composites to flames due to such fibres and polymers has limited their use in applications, especially where fire threat is imminent³⁰ and their tensile strength is diminished owing to several temperature-dependent softening processes. These softening processes are illustrated in [Figure 1](#).³¹

Generally, inorganic reinforcements such as carbon fibre (CF), glass fibre (GF), and basalt fibre (BF) are non-flammable. This is because the softening temperature of E-glass fibre is around 850°C, while carbon fibre can sustain high temperatures which most fibres usually cannot, and basalt fibres can resist up to 650°C.^{32–34} In the case of combustible fibres, the released gases, heat, and smoke may add to the fire propagation. Thus, the role of fibre reinforcement in the burning of composite laminates is significantly complex. The combustion of the composite can be attributed to the type of fibre, its quantity, orientation, fibre length, thermal conductivity, and size agent.^{35–37} During exposure to massive heat emitted from fire, the composite consisting of polymer matrix and flammable fibres will decompose thermally. Similarly, this thermal decomposition mostly happens with virgin

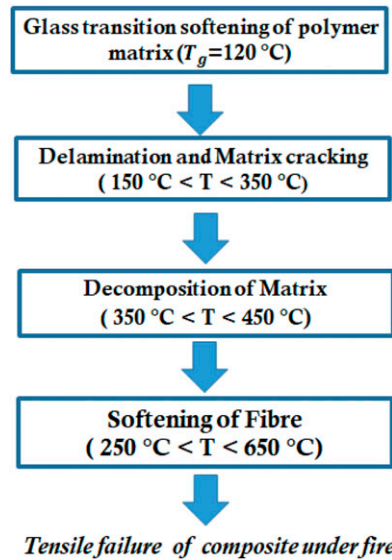


Figure 1. Softening process of basalt and glass fibre composites with elevating temperature.³¹

polymers. The details of the decomposition of composite materials include the formation of char, matrix softening, and material degradation. After that, matrix cracking alongside delamination can be observed. Then, material strength and stiffness are reduced leading to the de-bonding of fibres from the matrix.^{38–40}

In events where the composite laminate is directly exposed to the flame, as shown in [Figure 2](#), the fire-facing side is the first area to be damaged by flame and consequently, the heat will be transferred to the inside layers by conduction and heat diffusion. In the through-thickness direction, the heat transfer rate is significantly lower than that in the fibres direction. This is due to the higher heat conductivity of fibres than the polymeric matrix. Consequently, a temperature gradient across the composite material is produced and three different regions can be observed in its thickness direction. These regions are the hot surface region, the decomposition region under the first one, and the hind face region.⁴¹

Many failure mechanisms occur in composite laminates when they are subjected to various high-temperature ranges. Firstly, the failure mode is brittle, and fibres are still surrounded by the polymer matrix when the temperature is below the glass transition (T_g) of the polymer. So that, the temperature has a pronounced effect on the tensile properties of composite laminates. Secondly, when the temperature reaches the glass transition (T_g) of the polymer, the softening of the polymer happens leading to separate fibres fracture.⁴² That is, the laminate materials fail because of the polymer softening and gasification which is typically followed by fibre rupture. Hence considerable degradation occurs in the mechanical performance of composite laminates and part of the polymer is lost. Thirdly, by increasing the temperature up to the decomposition temperature of polymer (T_d),

virtually no polymer will be left considering that the resin reaches a temperature close to its self-ignition temperature, and the specimen bends freely. Finally, elevating the temperature to extreme values (i.e. 450°C–706°C), the polymer matrix will be entirely burned and a significant fraction of fibres will be oxidised.⁴³ The degradation mechanisms of composite laminates have been illustrated with the aid of scanning electron microscopy images (SEM) in Figure 3. As can be seen, by increasing the applied temperature, the polymer matrix begins to break down (i.e. it softens, cracks, and eventually burns), making the fibres visible and separate.

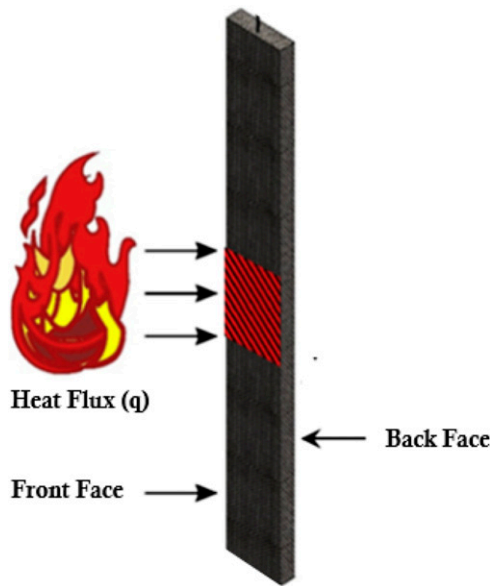


Figure 2. Exposure of a composite to radiant heat at a constant heat flux.^{31,41}

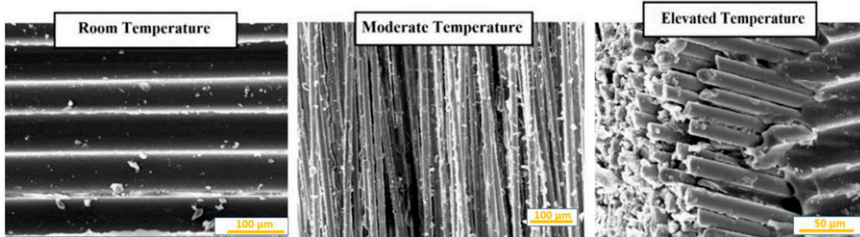


Figure 3. SEM micrographs of composite laminates after exposure to the temperatures ranged from approximately 20 to 700°C.⁴³

Further, in load-bearing applications, fire resistance is a significant property of composite laminates. This can be attributed to the composite mechanical properties as fire can severely compromise the structural integrity. Thus, considerable research work has been focused on improving the fire resistance of composites by employing various methods, composite material systems, and testing methodologies.

Test methods of fire response

Three main types of test facilities as listed in Figure 4 can investigate the response of composite materials to fire. To comprehend the fire resistance properties of composite laminates during the application, a number of test methods have been described at various scales and these testes are essential and considerable in industrial applications

Thermal gravimetric analysis. This is a small-scale test which makes use of small size samples (a couple of millimetres or milligrams). During the fire test, different atmospheres of either air or inert gas are used at various heating rates (typically between 2 and 20°C/min).⁴⁴ The conditions of heat transfer, its rate, temperature, surrounding environment, and heat transfer mechanism are the major controlling factors. The procedure of this test is generally similar to differential scanning calorimetric (DSC) analysis. Both types of test (TGA and DSC) are utilised to evaluate the curing response and glass transition temperature of polymer composite elements.⁴⁵

Micro-scale Cone Calorimeter (MCC). This test method is applied to determine the combustion behaviour of polymeric composites according to ASTM D7309-07 standard. Each sample with 4~8 mg mass is heated at a heating rate of 1°C/s from 90°C to 600°C for 30 s. During the decomposition process, the products of pyrolysis are generally moved to a combustion furnace in a nitrogen atmosphere at a high temperature. Here, pure oxygen is added in a sufficient amount and the complete combustion of pyrolysis products is carried out.⁴⁴ The heat emission rate is measured by assessing the oxygen concentration by using an oxygen analyser.^{46,47}

Pyrolysis Combustion Flow Calorimetry (PCFC). This technique is applied to study the fire response of polymer composites at microscale level. Samples of mass 2 mg undergo

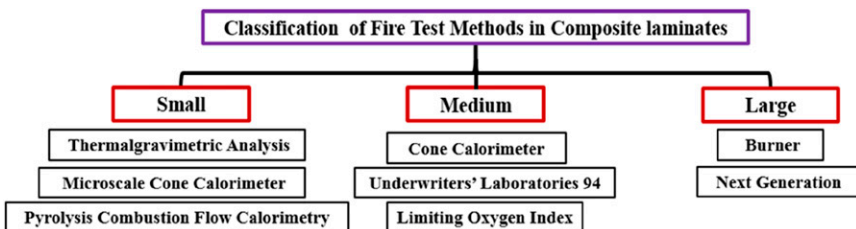


Figure 4. Test methods of fire behaviour and thermal stability of composite laminates based on different scales.⁵⁸

pyrolysis at 1°C followed by treating the pyrolysis products with an inert gas flux. The samples are treated with oxygen before putting them into a combustor for complete oxidation at 900°C. Finally, the heat release rate (HRR) is considered the single most important fire reaction property because the heat released by a burning material can contribute to the growth and spread of fire. Further, HRR is determined by several combustion processes, with the most important being combustion of hydrocarbon volatiles released from a decomposing composite.^{48,49}

Cone Calorimeter Test (CCT). This is the most reliable and frequently used test employed for evaluating the thermal combustion behaviour and fire performance index of composites. According to ISO 5660-1 standard, the Cone Calorimeter method is rated as the most significant tool for fire-testing of solid materials. The amount of energy generated during combustion is equal to 13.1 MJ per kg of oxygen. In application, in order to examine some material elements of an aircraft, often 50 kW/m² of heat flux is used.^{50–52}

Limiting Oxygen Index (LOI). The criteria of this test are based on test standards such as the ASTM D2863 and ISO 4589-2.^{52,53} This test is used to determine the lowest concentration of oxygen existing in an atmosphere of oxygen–nitrogen required to sustain the ignition and burning of vertically mounted composite samples. The suitable dimensions for the test specimen according to ASTM D2863-97 standard are 100 mm (length) × 6.5 mm (width) × 3.2 mm (thickness).⁵⁴

Underwriters laboratories 94 (UL-94). This test is known for vertical fire testing and has three sets of ratings. The first set is defined as V-0 in which the entire flaming time is not more than 10 s. The second set is referred to as V-1 and the complete flaming time is between 10 and 30 s; the cotton material, which is located beneath the sample, is not burnt. The final set is known as V-2 and the cotton material stabilizes during the test. V-0 exhibits the best performance among all three ratings.⁵⁵

Next generation (NexGen) burner. This method was developed by the Federal Aviation Administration (FAA) for large-scale material testing. The condition of the impinging flame should provide a heat flux of 116 kW/m² ± 10 kW/m² while maintaining an average temperature of 1100°C ± 80°C.⁵⁵ The design of the bench is suitable for conditions of burning quite similar to real-time applications such as composites decomposition. The samples being used for testing must hold out against a flame premixed with kerosene–air. If the exposed area of the sample resists fire without self-ignition for more than 5 min, it is recognised as fire-resistant; whereas the material is considered fire-proof if it withstands for 15 min.^{56,57}

Modelling of flammability in composite laminates

Although the demand for composites in modern aeronautical applications is on the rise, their sensitivity to fire is limiting their use for widespread applications. It has been recognized that the exposure of composites to fire results in stiffness losses and

eventually lowers the load-carrying capabilities of composites. Thus, in order to deal with the fire resistance and flammability of composite laminates, multi-scale modelling techniques are required. Furthermore, these models can replace real-time expensive testing by some approximation, and the damage parameters can be predicted. The general purpose of computational models and simulation of fire resistance in composites is to develop methodologies for measuring exposure of composite materials to flame retardants and flammability, validate techniques through correlation with experimental results, and finally use these simulation tools to analyze typical events to get a better understanding of the characteristics of flammability of composite laminates. The released heat associated with the ignition of gases produced at the surface of a polymer matrix composite has been modelled and investigated under pilot flame.⁵⁹ Studies have been conducted on the characterisation of the fire reaction behavior of structural composite materials, and huge data on time-to-ignition, rate of heat release, limits of oxygen index, flame spreading, density, and toxicity of smoke have been extracted.^{60–62} Organic composites become highly sensitive and reactive at high temperatures compared with structural materials like reinforced concrete, aluminium alloy, and steel because the composites contain organic matrix and organic fibres such as aramid, polyethylene, and polypropylene. Generally, the composite laminates are often utilized in structures like glass–vinyl ester, glass–polyester, carbon–epoxy, and carbon–thermoplastic materials. However decomposition occurs on exposure to a fire at relatively high temperatures (more than 100°C), and heat, smoke, and fumes are released. Studies have been conducted on the characterisation of the fire reaction behaviour of structural composite materials, and huge data on time-to-ignition, rate of heat release, limits of oxygen index, flame spreading, density, and toxicity of smoke have been extracted.^{63–72} Moreover, researchers have developed theoretical models to predict some fire response properties of laminated composites such as ignition time and the amount of heat released.^{73–75} To simulate the fire performance of the composite structures, the building models should comprehend the thermal, chemical, physical, and failure processes occurring in the composites during a fire event. In modelling, the accurate analysis and representing numerous processes occurring simultaneously during a fire is a big challenge. The analysis is complex given the number of the processes happening at the same time; thus, a true understanding of the processes' interaction inside the composite laminates is crucial to analyse the fire structural behaviour. Researchers have used thermal-mechanical models to determine the temperature distribution, decomposition process, softening of the material, and failure of laminated composites and sandwich composites.^{76–86} Meanwhile others adopted models to calculate the post-fire properties of composite laminates.^{87–95} There has been significant progress with regard to the validation of models depending on fire structural tests which include the development of comparatively low-cost test methods. To evaluate the composite degradation in addition to the production of pyrolysis, the thermal-mechanical models take into consideration the thermal, chemical, and physical changes in the solid phase regardless of material type. A direct flame was utilized to simulate the ignition of the combustible gases and emissions near the surface. Thus, a carbon-epoxy composite with a small-scale fire experiment was performed to verify the prediction of the model. The model could

predict the time to ignition and the temperature of the back face of the sample without using empirical methods.⁵⁹ For different periods of fire exposure, the evaluation of the composite temperature and density throughout the material thickness can be predicted using this model (see Figure 5).⁵⁹

Finite element and finite volume methods (FEM & FVM) were coupled to develop a fire-structure model,⁹⁶ whereby the essential changes in the physics of the material can be captured. A multi-physics scheme was adopted where the essential physical changes due to the combustion and thermo-mechanical variation in the structure, especially for natural FRCLs, has been observed. At the solid-gas interface, the concept of adiabatic surface temperature was also utilized as a new method to transfer data between fire and thermal/structural models. Under both mechanical and thermal loads, the model was able to predict the deformation (as shown in Figure 6), temperature, and stress distribution of composite beams.

A thermo-mechanical model was presented for the analysis of a laminated composite shell exposed to fire.⁹⁷ The temperature distribution across the shell thickness was determined by using a one-dimensional thermal model. The thermal model was based on the following governing equation which was proposed by Henderson et al.⁹⁸

$$\rho C_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) - w_g C_{pg} \nabla T - \frac{\partial \rho}{\partial t} (Q_p + h_s - h_g),$$

Where C_p is the specific heat, T is temperature, k is the thermal conductivity, h_g is the specific enthalpy of the gas, w_g is the mass flux of the gas, C_{pg} is the specific heat capacity of the gas, Q_p is the energy source of the polymer, and h_s is the specific enthalpy of the solid.

Thermal deformation has been taken into account, and the numerical results were validated and compared with experimental data. The behaviour of composite laminates under fire was also predicted by a thermo-mechanical model.⁹⁹ In this model, the three layers of composite laminates have been taken into consideration and an ordinary state-based thermo-mechanical model was developed. Thermal changes in properties have also

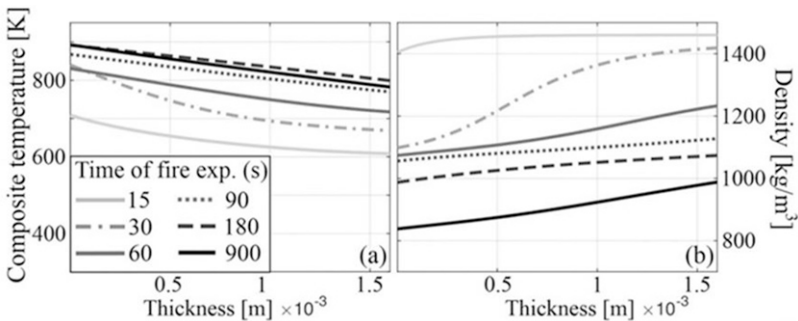


Figure 5. Prediction of composite temperature and density through its thickness.⁵⁹

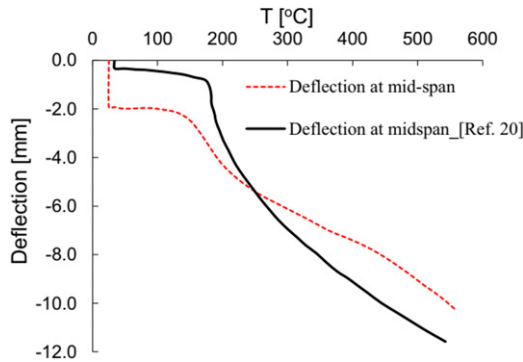


Figure 6. Deflection of a steel beam subjected to heating from one side.⁹⁶

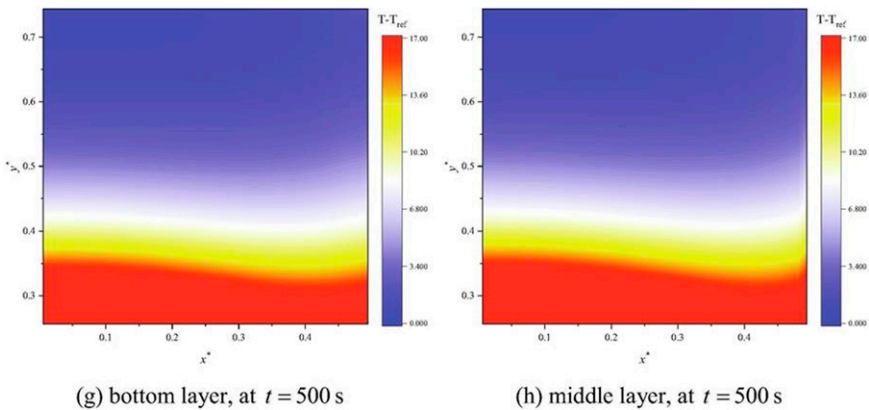


Figure 7. Temperature variation in a composite with respect to a reference temperature.⁹⁹

been taken into account. This enables the prediction of heat conduction, temperature (as shown in Figure 7), and mechanical deformation in the composite. Here, the fire was modelled by heat-conducting fluid. The influence of hot gas and direct contact with fire on composite thickness degradation was investigated.

The thermo-mechanical damage of glass composite laminates in fire has been predicted and radiative environment and high temperature were simulated by using a 3D thermal approach¹⁰⁰; the constituents of the laminate such as fibre, polymer, and char have been assumed as a homogeneous state. The time to failure of thermal damage, which was extracted from the model, has shown a reasonable agreement with experimental data for the sandwich composite panel, as depicted in Figure 8.

The influence of compressive loading under fire conditions for a basalt composite laminate was investigated analytically and experimentally.¹⁰¹ The fire structural performance of basalt laminate was compared with E-glass laminates keeping the same

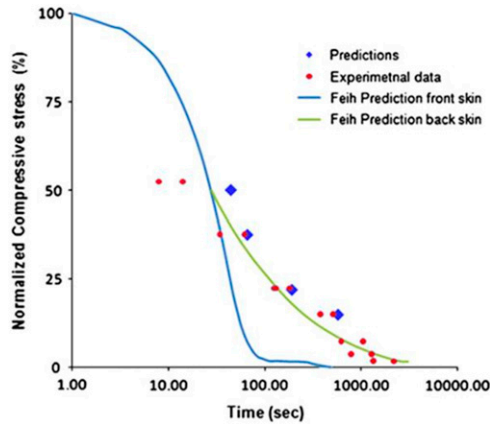


Figure 8. Prediction of time-to-failure under variable compressive load and a heat flux of 50 kW/m^2 .¹⁰⁰

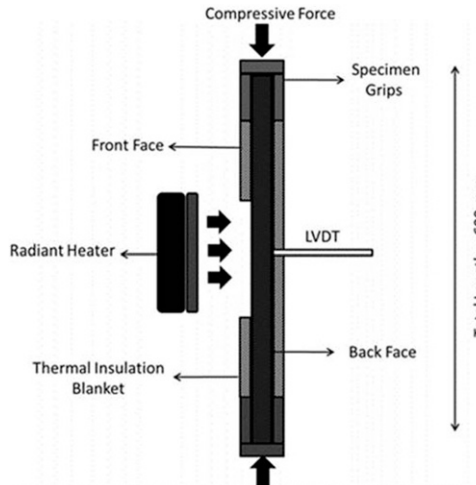


Figure 9. Schematic drawing of the experimental facility.¹⁰¹

polymer matrix (polymer), fibre volume fraction, and ply orientation for both types of laminates. Experimental results were achieved by exposing one side of the laminates to axial compression and radiant heat as shown in Figure 9. It was found that the collapse in fibres occurred due to global buckling and natural damage when exposed to fire. The glass

laminate showed better compressive performance and higher fire resistance compared to the basalt laminate. This was attributed mainly to the relatively high thermal absorptivity of basalt, which was due to reaching high temperatures in a relatively short time when it was exposed to fire.

Fire-resistance of composite laminates

Fire resistant composites are materials that resist the fire spreading, while their mechanical or structural integrity (load capacity bearing property) is almost constant in the case of fire exposure. The assessment of these materials can be carried out by heat insulation, burn-through resistance, and structural integrity that are considered as the main fire-resistance properties.^{102,103} The heat insulation property is the factor that controls the conduction of heat transfer rate through a material during combustion.^{104,105} Burn-through is known as the period of time necessary for the flame intrusion to enter from one side and pierce to the opposing side.¹⁰⁶ Mechanical integrity is known as the capability of a material to retain its mechanical properties like creep resistance, stiffness, and strength during burning.¹⁰⁷

Over the last few years, polymer composites have illustrated remarkable potential in numerous applications serving as essential structural elements, predominantly in aircraft, automobiles, transport, railways, construction sectors, and furniture.^{108,109} However, in terms of fire safety, they showed disadvantages owing to their high flammability leading them to deform easily because of structural failure resulting from stiffness and creep resistance losses.^{106,110} The fire behaviour of composite materials, when they are exposed to flame, can be analysed by fire response and fire resistance.^{111,112} Even if the supplied fuel has been suppressed or extinguished, hydrocarbons in the polymer composites would serve as alternate sources of fuel to maintain flame propagation.¹¹³ Hence, these

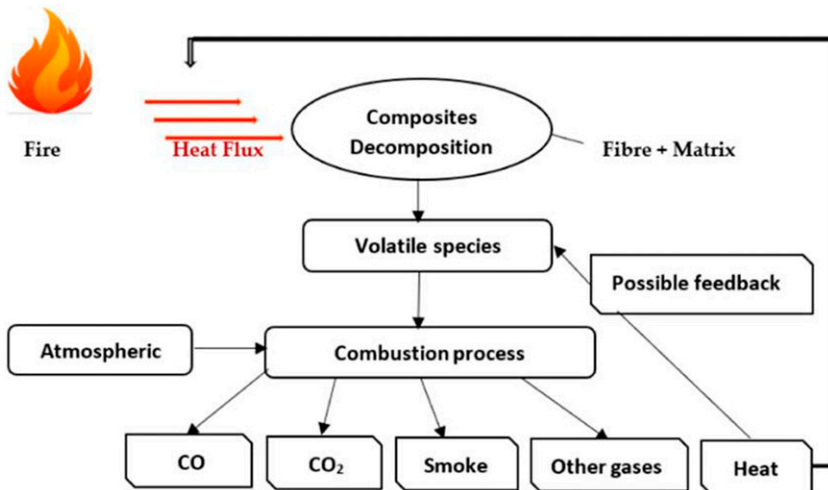


Figure 10. Thermal decomposition cycle of polymer composites.⁵⁸

composites experience a thermal decomposition process on exposure to fire due to a number of chemical reactions occurring simultaneously.^{48,114,115} The decomposition process occurs when chains of polymers of high molecular weight start to break down into volatiles with lower molecular weight. These volatiles infiltrate the flame zone as shown in Figure 10.^{49,116}

Several researchers have focused on the concept of flame retardancy by way of improving the fire retardant properties of composites, reducing their flammability and improving their thermal durability.^{117,118} The following details are explained the approaches that can be considered for enhancing the fire resistance of composite laminates.

Methods of improving fire-resistance of composite laminates

Conventional composite laminates exhibit relatively high sensitivity to fire and tend to delaminate, compromising their mechanical performance. Thus, several different approaches have been adopted to investigate their flammability and improve their thermal stability. These processes may be broadly classified into methods that enhance the fire resistance of polymer and techniques that modify the fibre architecture. The FR additives can be included into polymers with different scales such as nano- or micro-sized fillers to boost their FR response.^{119,120} Further, fibre alteration approaches incorporated either yarns hybridization or layers hybridization.¹²¹

Improving fire-resistance via toughening of matrix

Polymeric, ceramic, and metallic are main matrices in the composites materials. The most common in the manufacturing of these composites are the polymeric matrices, which divided into thermoplastics and thermosets matrices.^{122,123} The using of thermoplastic matrices can increase the toughness and damage tolerance of composites.^{124,125} However, they provide lower stiffness and their manufacturing cost is higher compared with the thermosets based composites.^{126,127} Meanwhile, the thermoset resins, such as epoxy are most widely used in manufacturing of composite materials due to their great mechanical and good thermal properties.^{128,129} In this regards, the thermosets based composites have been selected in this review.

Thermoset matrices (e.g. epoxy polymers) have outstanding properties such as the ability to impregnate the fibre reinforcement properly and better adhesion leading to an outstanding mechanical performance, improved chemical and electrical resistivity, and less shrinkage during the curing process. However, the combustibility of epoxy polymers is a key issue in structural application since a fire event implicates not only risks to health but also a reduction of mechanical properties.^{22,23} To meet the requirements of the application, their fire resistance properties must be enhanced without compromising the other essential mechanical characteristics and thermal properties. Besides, it is critical to consider the environmental issues as well. Specifically, the formulation must be pre-impregnable for a proper degree of tack and drape, have suitable modulus and glass transition temperature, and have increased fire resistance compared to baseline matrices.¹³⁰ The fire resistance of matrices can be modified by using different techniques.

These techniques vary from simple methods like incorporating additives into a polymer (nano- and micro filler) or coating heat-resistant materials, which involve chemically modifying the polymer or heat induction to the surface of the composite to influence intumescence.¹³¹

Micro-phase toughening. In general, the FRs, which are incorporated in polymers of composites, are broadly divided into two major classes: the first is known as additive compounds and the second is defined as reactive compounds.¹³² The additive FRs are added into the polymeric polymer by course processing while no chemical reaction occurs between them. These chemicals include bromine, boron, chlorine, aluminium, phosphorus, and antimony.¹³² Many additives work as hydrated metal salts which go through endo-thermal decomposition on exposure to fire and hence reduce the rate of total heat release of a polymer matrix.^{133,134} Moreover, some other additives also emit water vapours during thermal decomposition that dilute the concentration of combustible emission gases discharged into the flame zone.^{58,135} In contrast, the reactive fire retardants are integrated into the network of the polymer molecular structure through a co-polymerisation process.^{136,137} Halogens (i.e. bromine, chlorine), melamine, phosphorus and inorganic compounds are the main structures of reactive compounds. However, the halogen source is the most effective FR, for both matrix and fibre.^{138–140} They operate by releasing reactive chloride or bromide radicals into the flame zone which provide the highest flame resistance by disturbing the oxidative combustion process of the flammable volatiles.^{141,142} But in recent times, restrictions have been applied on the use of halogen-based FRs on account of health and environmental issues associated with them. Phosphorus-based compounds are also quite effective FRs that decrease the emission of flammable gases from the degrading polymer by increasing char production. The selection of suitable flame retardant depends on various factors such as cost, temperature of decomposition, weight and compatibility between polymer and FR. In order to overcome the adverse effect of decreased mechanical properties of some filler additives, surface treatment of the particles is done to enhance the chemical interaction with the polymer polymer. Some filler compounds increase the concentration of smoke particles and toxic fumes during degradation of the composite materials. Therefore, to improve the fire resistance while avoiding the undesirable consequences of toxicity, smoke, and reduced mechanical strength, it is imperative to adopt an approach of incorporating two or more FRs in combination into the polymer composite materials (this process is defined as the intumescent fire-retardant system).

Several researchers have focused on the use of halogen-free fire-retardants in polymer systems. Shi et al. studied the heat conduction and flame resistance of epoxy composites by adding Si_3N_4 and $\text{Al}(\text{OH})_3$ (Aluminium Tri-hydroxide, ATH) fillers.¹⁴³ Their findings illustrated that Si_3N_4 significantly increases thermal conductivity, whereas ATH has a great effect on the fire resistance of epoxy. The effects of APP (Ammonium Polyphosphate) and melamine cyanurate (MC) on the flammability and mechanical performance of glass fibre-reinforced epoxy composites were studied by Lim et al.,¹⁴⁴ where APP illustrated higher flame retardant properties compared to MC.

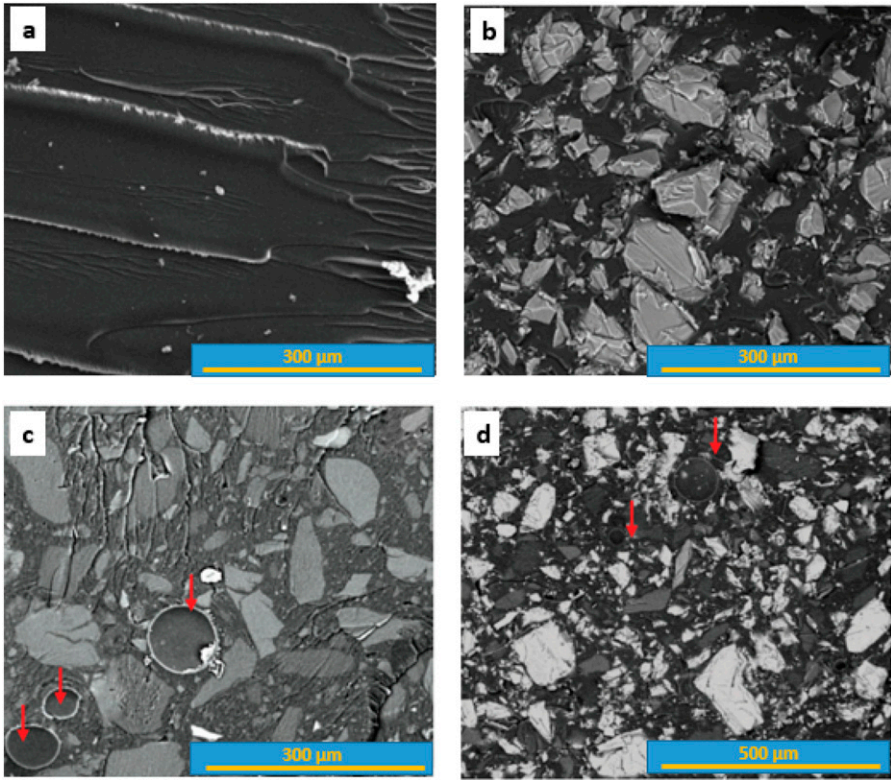


Figure 11. Scanning electron images presenting effective dispersion of AG and APP phases: (a) neat epoxy, (b) 20 APP, (c) 20 AG, and (d) 5AG-15APP samples.¹¹⁹

Riahipour et al.¹¹⁹ investigated the influence of silica AG (20 nm) and APP (5 μm) on mechanical, thermal and flame-resistant properties of epoxy-based composites as shown in Figure 11. Their results showed that APP decreased the burning rate of epoxy composite with higher thermal stability.

Wang et al.¹⁴⁵ studied the influence of adding APP and ATH agents on the thermal and fire-retardant properties of PVA (polyvinyl alcohol)/clay aerogels. They did not find a noticeable effect resulting from combining APP and clay AG on the onset of polymer decomposition; however, a significant reduction in aerogel decomposition rate was noticed between 250°C and 500°C.

Nano-phase toughening. The use of nano-sized organic and inorganic particles in epoxy polymers to improve their fire, mechanical, and physical properties has drawn attention in recent years because of their good dispersion and strong interfacial interaction.¹⁴⁶ Recently, Epoxy/SiO₂ nano-composites are widely used in fire resistance applications due to the high stability of silica at high temperatures and the strong linkage between EP and

SiO₂.^{147–149} Vu et al. and Kui Wang et al. studied the influence of silica after addition to 9,10-dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO) on the flammability and mechanical properties of an EP/silica system^{150,151} and reported improvement in fire resistance of the EP/silica system.

Recently, graphene is gaining attention as a halogen-free fire retardant for epoxy polymer owing to its 2D structure of a carbon layer as a physical blockade to impede the escape of volatile products.¹⁵² However, the flame retardant performance of graphene by adding it alone to the polymer matrix is still unsatisfactory because of its flammability in the air atmosphere.¹⁵³ The limiting oxygen index (LOI) is a parameter that is used for evaluating the flammability performance of various types of materials according to ASTM D2863. Moreover, LOI measures the minimum oxygen concentration contributing to the combustion reaction. Thus, a material with a high value of LOI is less likely to burn. The LOI of these samples was measured to comprehend the combined impact of the fillers on the polymer composites.¹⁵⁴ Guo YQ studied the effect of flame retardant properties of graphene, graphite oxide (GO), and functionalized graphite oxides (FGO) on the epoxy composite.¹⁵⁵ It was found that the performance of graphene composites is better than graphite oxide composites.

Guo et al.¹⁵⁵ incorporated graphite (EG), graphene, GO, organic phosphate, and FGO into an epoxy resin (EP) matrix. Using transmission electron microscopy, the structure of the composites was characterized to illustrate dispersion without large aggregates. The flame retardancy was investigated using a micro combustion calorimeter. The results illustrated that EP/graphene as well as EP/FGO composites exhibited better flame retardancy than EP/GO composites with a maximum reduction of 23.7% in peak-heat release rate when containing 5 wt % FGO and a maximum reduction of 43.9% at 5 wt % loading of graphene.

Carbon nano-tubes (CNTs) have been used as common nano-particles in nano-composites for fire resistance. They can be categorized into single-walled (SWCNT), double-walled (DWCNT), and multi-walled (MWCNT).¹⁵⁶ These materials have been adopted to decrease the flammability of a number of polymers for example ethylene vinyl acetate (EVA),¹⁵⁷ polystyrene (PS),¹⁵⁸ polypropylene (PP),¹⁵⁹ and polyimide 6 (PA).¹⁶⁰ CNTs, due to their high aspect ratio, percolate to form a network at a low loading level in the polymer matrix and lead to significant improvement in fire retardancy. So that, in composites, they largely contribute to increasing the fire resistance.¹⁶¹ However, the dispersion of these particles inside the polymer system and the chemical reaction between the CNTs and the epoxy polymer matrix is a major problem that needs to be resolved. Owing to the high surface area, the CNTs create a robust van der Waal bond between individual tubes generating agglomerates and holding them in bundles as illustrated in Figure 12.¹⁶²

Although the CNT agglomerates can improve the electrical conductivity of composite laminates,¹⁶³ they can cause degradation of certain properties of composites.¹⁶⁴ For instance, the stiffness and strength of nano-composites are the most pronounced weakening effects caused by CNT agglomerates.^{165,166} Moreover, agglomerates cause very low solubility of CNTs in most solvents, leading to inhomogeneous dispersion within a surrounding matrix.¹⁶⁷ Thus, the homogeneous dispersion of CNTs inside the

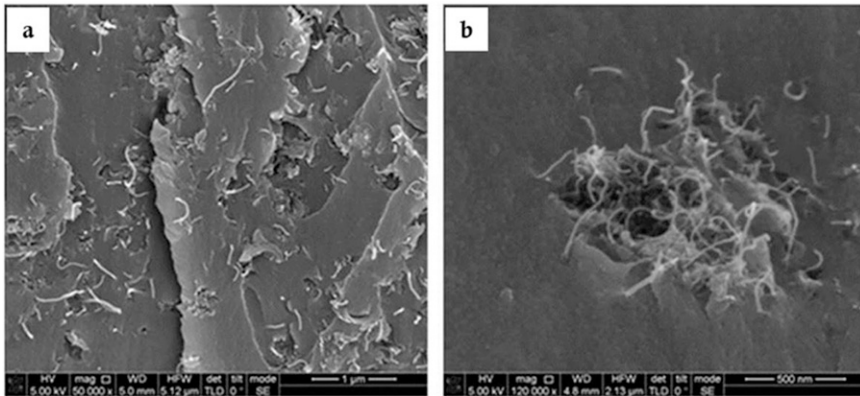


Figure 12. SEM micrographs illustrating the dispersion of carbon nano-tubes in the fracture surface of a carbon fibre composite: (a) homogeneous dispersion for CNTs and (b) CNTs agglomeration.¹⁶⁹

matrix is essential to prevent secondary agglomeration and increase the specific surface area of CNTs during the composite manufacturing.¹⁶⁸

Table 1 presents the promising results that were achieved by researchers by adding nanoparticles into matrix materials.

In summary, the hybridisation of a matrix can be achieved mainly through micro- and nano-particles to improve the flame resistance of composites. However, homogeneous and stable dispersion of nano-particles in the matrix is a major obstacle that needs to be resolved.

Improving fire-resistance by reinforcement construction

Fibre-reinforced polymer composites are a class of composite materials that are made from a polymer matrix reinforced by fibres. These fibres have diameters ranging from a few micro-metres to many hundreds of micro-metres. The reinforcing fibres usually serve to give strength and stiffness to the composite laminates.¹⁸⁰

A composite produced by using two different types of fibres with a matrix material is often called a fibre-hybrid composite. Hybrid composites exhibit some specific advantages compared to conventional composites such as thermal distortion stability, good strength, stiffness, fire resistance, reduced weight, cost, notch sensitivity, improved fatigue resistance, fracture toughness, and impact resistance.^{181,182} Fibre-hybrids can be classified into three various classes: Figure 13 shows various configurations of fibre-hybridisation: intra-yarn, intra-layer, and inter-layer.^{183–185} It is worth mentioning that these classes are often referred to as fibre-by-fibre or commingled or intermingled, yarn-by-yarn and layer-by-layer or interlaminated respectively.^{186–191}

Fire resistance is considered as a functional property of composite laminates, and fibre hybridisation is an approach through which it can easily be enhanced.^{192–194} Most of the

Table I. Reported work on the addition of nanoparticles into composite materials.

Chemical or filler names	Fire test	Name of property that improved	Type of composite laminates	References
1-Alumina nanoparticles (~ 13 nm)	TGA	<ul style="list-style-type: none"> • Slight reduction in heat release rate. • Anti- oxidizer agent for the char and carbon fibre. 	Carbon fibre composites	170
2- Nanosized calcium silicate (~ 100 nm)	LOI	<ul style="list-style-type: none"> • Increase thermal stability. • Improve the fire resistivity of phenolic/cotton fabric reinforced polymer composite. 	Phenolic/cotton fabric reinforced polymer composite	171
3- SiO ₂ nanoparticles (~ 33.58 nm)	TGA	<ul style="list-style-type: none"> • Increased amount of thermally stable carbonaceous char. • Improve the thermal stability and mechanical performance of EP. 	Epoxy	151
4- Graphene nano platelets	CCT	<ul style="list-style-type: none"> • Decrease in heat release rate. 	Polyvinyl chloride	172
5- Nano-aluminium hydroxide	LOI UL-94 CCT	<ul style="list-style-type: none"> • Decrease heat release rate by 56%. • Formation of an intact and homogeneous char during combustion. 	Polypropylene	173
6- Magnesium hydroxide nanoparticles	CCT	<ul style="list-style-type: none"> • Decrease heat release rate by 72%. • A uniform and continuous residue layer for the PP/MH nanocomposite is formed during burning. 	Polypropylene	174
7- Carbon nanotubes	LOI UL-94 CCT	<ul style="list-style-type: none"> • Increased thermal stability. 	Epoxy	175,176
8- Modified nano-Sb ₂ O ₃	TGA	<ul style="list-style-type: none"> • Catalytic char formation. 	Poly butylenes terephthalate) (PBT) composite	177
9- Titanium carbide nanosheets with melamine cyanurate.	CCT	<ul style="list-style-type: none"> • 40% reduction in the peak of heat release rate. 	Thermoplastic polyurethane (TPU)	178
10- Organo-intercalated layered double hydroxides.	TGA	<ul style="list-style-type: none"> • Enhanced thermal stability. 	Ethylene vinyl acetate (EVA)	179

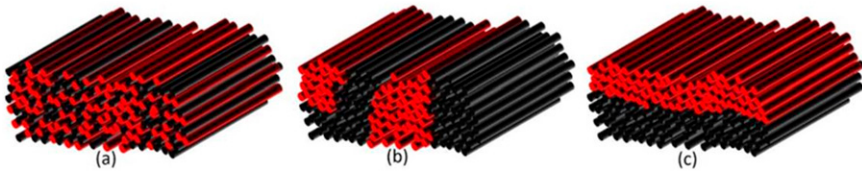


Figure 13. Configurations of fibre-hybridisation: (a) intra-yarn, (b) intra-layer, and (c) inter-layer.¹⁸⁵

high-performance fibres such as aramid fibres offer low flammability and do not melt easily but carbonise on exposure to fire. As a result, a char layer is produced which is similar to one resulted by phenolic polymer.^{195–197} Kim et al.¹⁹⁷ studied the influence of the addition of aramid fibre layers to a sandwich made from glass fibre/phenolic skins. The results showed that the post-fire tensile strength of the skins increased by 95% and the post-fire flexural strength of the sandwich improved by 240%. The layer lay-up also played an important role. They observed that the lay-up of aramid/glass/aramid had a substantially lower rate of fire propagation than the lay-up of glass/aramid/glass.¹⁹⁴ Xiaoye Cong et al.¹⁹⁸ investigated the mechanical performances and fire protection behaviour of composites consisting of thin-ply carbon fibre prepreg and FR mats. These FR mats include an expandable graphite, mineral wool and glass fibre to generate a thermal barrier. The results confirmed that composites with flame retardant mats achieved higher fire protection according to the EN 45545-2 standard, and high value of average rate of heat emission (MARHE).

Additionally, there is a growing interest in hybrid laminates made from the combination of synthetic fibres (like glass fibre) and natural fibres aiming to manufacture composites that are environmentally friendly and less flammable.¹⁹⁹ Nurul et al.¹⁹² showed that the bamboo-glass hybrid polypropylene composites are thermally more stable before starting to decompose at 275°C and fully degrading at 400°C compared to the glass-polypropylene (GPP) composites.

A multi-layer polymer-metal laminate (PML) can also be used for thermal insulation in lightweight structural materials such as aluminium and carbon fibre reinforced composites. Fire test findings have shown a decrease in substrate temperatures and a substantial increase in time to failure under load in these hybrid laminates. This system of protection, obtained from materials such as intumescent coatings or ceramic fibre mat against fire offers an equivalent or even superior approach compared to conventional fire protection.²⁰⁰

Improving the interface region between polymer matrix and reinforcement. The fibre-polymer interface, which is formed during the composite curing process, can mainly be classified into two phases: the first phase is full wettability of fibres by polymer through the impregnation process, while the second phase is chemical bonding that occurs during the cross-linking reaction of polymer during the solidification process.²⁰¹ On exposure of a composite to fire, the burning behaviour of interfacial polymer is much more rigorous because of the wicking effect. At the combustion temperature, the polymer would melt,

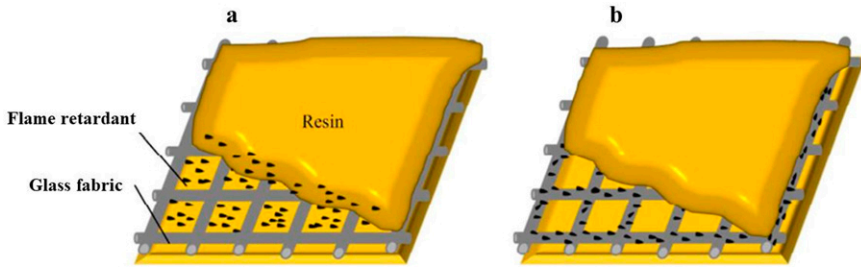


Figure 14. The distribution of flame retardant at (a) bulk and (b) interfacial region.²⁰³

wet the interfacial fibres, and spread on the fibres' surface leading to the rapid and inclined flow of the polymer melt along the fibres' surface towards the fire zone. This phenomenon will expedite the fuel supply and intensify the combustion, particularly in fibre-reinforced thermoplastic composites. Thus, the combustion rates at the interfacial regions and within matrix materials are considerably different. To deal with the above issue, interfacial FR changes of fibres by adopting physical or chemical approaches have been suggested. These approaches can increase the fire retardancy without altering the process or composite molding techniques while maintaining their mechanical characteristics.^{202,203} These approaches are particularly attractive for composites reinforced with natural and organic fibre as the fibres can easily be functionalized or incorporate FR into their matrix.^{204,205}

The FR modified fibres can produce a very high concentration at interfacial regions, resulting in high surface roughness and lower surface energy compared to the original fibres. Further, the flame retardant fibres can react with the matrix to produce chars that grow along fibres at combustion temperature producing a more rough and inert surface of fibres. As can be seen in Figure 14, the residues containing fibres and chars can effectually block the adsorption, wetting the fibres, spreading along and flow of the polymer melt in interfacial regions, which can weaken and even stop the wicking process and significantly enhance the flame retardancy of composite.^{206–208} Most thermosets do not experience wicking action during combustion compared to thermoplastics. Thus, the produced chars can grow along with the fibres particularly for phosphorus-containing FRs making an effective fibre shield. The high-quality shield consisted of a high-strength skeleton (fibres) and condensed fillings (chars) that can be used to block off oxygen, heat, and degraded volatiles.^{202,209,210} In terms of the amount of char for integrating fibres together, it is considerably smaller than achieving a compact protective coating independently. More significantly, the shield strength owes to the integration of fibres and chars. Carbon nano-materials such as graphene, carbon nanotubes and carbon black, are significantly used to enhance the interface area between the polymer matrix and the reinforcement; leading to improve the polymers' flammability, mechanical properties and conductivity.²¹¹

Summary and conclusions

In recent times, the fire-safe design of composite laminates has gained significant attention due to the increasing demands of composites in numerous applications. This research review has illustrated the response and susceptibility of composite laminates when they are exposed to fire events. A considerable amount of literature has been highlighted that reveals the failure mechanisms occurring in composite laminates when subjected to different elevated temperature ranges. In addition, various test methods have been discussed in this paper to study the fire behaviour of composite laminates based on their flammability and the rate at which flammable and toxic gaseous elements are discharged. This review has also broadly enclosed the prediction of fire performance and induced damages extended to composite laminates in terms of numerical approaches to aid understanding of the complex phenomena happening simultaneously in the composite and enable estimating the consequences of flammability on composites.

The prime focus of this study has been to present insightful literature on improving the flame resistance and thermal stability of composite materials via multi-scale hybridisation techniques. These approaches may broadly be divided into methods that improve the fire resistance of polymer and methods that modify the reinforcements. Polymer-toughening methods include incorporation of micro- and nano-particles within the polymer systems. While, fibre alteration methods, which are including hybridisation approaches either at the yarn level or in layers have been discussed. Finally, the hybrid layer composite laminates have also been reviewed in this paper highlighting their influence on the flammability and thermal stability of composite laminates.

Further, the research work could possibly be extended for selective hybridization at matrix, reinforcement and layers levels to manufacture advanced composite laminates and investigating their response to fire by using Fire resistance test methods. Moreover, numerical analysis with aiding Abaqus software can be adopted for comparison with experimental results

Nomenclature

APP	Ammonium Polyphosphate
ATH	Aluminium Trihydroxide
BF	Basalt Fibre
CF	Carbon Fibre
CNT	Carbon Nano-Tubes
DOPO	9,10-dihydro-9-oxa-10-phosphaphenanthrene-10- oxide
DWCNT	Double-Walled Carbon Nano-Tubes
EG	Graphite
EVA	Ethylene Vinyl Acetate
FEM	Finite Element Method
FGO	Functionalized graphite oxides
FR	Flame Retardant

FRCL	Fibre-Reinforced Composites Laminates
FVM	Finite Volume Method
GF	Glass Fibre
GO	Graphite oxide
GPP	Glass–Polypropylene
HRR	Heat Release Rate
LOI	The limiting oxygen index
MARHE	Maximum Average Rate of Heat Emission
MC	Melamine Cyanurate
MWCNT	Multi-Walled Carbon Nano-Tubes
PA	Polyimide 6
PML	Polymer Metal Laminate
PP	Polypropylene
PS	Polystyrene
SWCNT	Single-Walled Carbon Nano-Tubes
Td	Decomposition Temperature of Polymer
Tg	Glass Transition Temperature of Polymer

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References

1. Forintos N and Czigany T. Multifunctional application of carbon fiber reinforced polymer composites: electrical properties of the reinforcing carbon fibers—a short review. *Compos B Eng* 2019; 162: 331–343.
2. Yu J, Cui Z, Lu J, et al. Integrated hierarchical macrostructures of flexible basalt fiber composites with tunable electromagnetic interference (EMI) shielding and rapid electro-thermal response. *Compos B Eng* 2021; 224: 109193.
3. Shi L, Song G, Li P, et al. Enhancing interfacial performance of epoxy resin composites via in-situ nucleophilic addition polymerization modification of carbon fibers with hyperbranched polyimidazole. *Compos Sci Technol* 2021; 201: 108522.
4. Kumar S and Singh K. Tribological behaviour of fibre-reinforced thermoset polymer composites: a review. *Proc Inst Mech Eng Part L* 2020; 234(11): 1439–1449.

5. Mlýnek J, Petrů M, Martinec T, et al. Fabrication of high-quality polymer composite frame by a new method of fiber winding process. *Polymers* 2020; 12(5): 1037.
6. Mittal G, Rhee KY, Mišković-Stanković V, et al. Reinforcements in multi-scale polymer composites: processing, properties, and applications. *Compos B Eng* 2018; 138: 122–139.
7. Gowda TY, Sanray M, Bhat K, et al. Polymer matrix-natural fiber composites: an overview. *Cogent Eng* 2018; 5(1): 1446667.
8. Song B, Wang T, Wang L, et al. Interfacially reinforced carbon fiber/epoxy composite laminates via in-situ synthesized graphitic carbon nitride (g-C₃N₄). *Compos B Eng* 2019; 158: 259–268.
9. Chen H, Deng C, Zhao Z-Y, et al. Novel piperazine-containing oligomer as flame retardant and crystallization induction additive for thermoplastics polyurethane. *Chem Eng J* 2020; 400: 125941.
10. Zhao X, Chen L, Li DF, et al. Biomimetic construction peanut-leaf structure on ammonium polyphosphate surface: improving its compatibility with poly (lactic acid) and flame-retardant efficiency simultaneously. *Chem Eng J* 2021; 412: 128737.
11. Kim Y-O, Cho J, Kim YN, et al. Recyclable, flame-retardant and smoke-suppressing tannic acid-based carbon-fiber-reinforced plastic. *Compos B Eng* 2020; 197: 108173.
12. Chen J, Wang J, Ding A, et al. Flame retardancy and mechanical properties of glass fibre reinforced polyethylene composites filled with novel intumescent flame retardant. *Compos B Eng* 2019; 179: 107555.
13. Toldy A, Szolnoki B and Marosi G. Flame retardancy of fibre-reinforced epoxy resin composites for aerospace applications. *Polym Degrad Stabil* 2011; 96(3): 371–376.
14. Branca C, Di Blasi C, Galgano A, et al. Thermal and kinetic characterization of a toughened epoxy resin reinforced with carbon fibers. *Thermochim Acta* 2011; 517(1-2): 53–62.
15. Lei Z, Cheng C, Yin B, et al. Low-velocity impact responses and failure mechanisms of CFRP after fire exposure. *Composites Communications* 2022; 34: 101277.
16. Lei Z, Ma J, Sun W, et al. Low-velocity impact and compression-after-impact behaviors of twill woven carbon fiber/glass fiber hybrid composite laminates with flame retardant epoxy resin. *Composites Structures* 2023; 321: 117253.
17. Vieille B and Coppalle A. Influence of temperature degradation on the low velocity impact behavior of hybrid thermoplastic PEEK laminates. *Journal of Thermoplastic Composite Materials* 2023; 37(1).
18. Mirmira SR. *Effective thermal conductivity of fibrous composites: experimental and analytical study*. College Station, TX: Texas A&M University, 1999.
19. Bulut Y and Erdoğan ÜH. Usability of cellulose based natural fibers as reinforcement materials in composite manufacturing. *Biology* 2011; 82.
20. D Soyaslan D. High structural insulation composite material development with electromagnetic protection effect reinforced with carbon fibers and particles. *J Ind Textil* 2021; 51(3): 424–434.
21. Kamble M, Lakhnot AS, Bartolucci SF, et al. Improvement in fatigue life of carbon fibre reinforced polymer composites via a nano-silica modified matrix. *Carbon* 2020; 170: 220–224.

22. Kandola BK, Horrocks A, Myler P, et al. Mechanical performance of heat/fire damaged novel flame retardant glass-reinforced epoxy composites. *Compos Appl Sci Manuf* 2003; 34(9): 863–873.
23. Mouritz A, Feih S, Kandare E, et al. Review of fire structural modelling of polymer composites. *Compos Appl Sci Manuf* 2009; 40(12): 1800–1814.
24. Huo S, Song P, Yu B, et al. Phosphorus-containing flame retardant epoxy thermosets: recent advances and future perspectives. *Prog Polym Sci* 2021; 114: 101366.
25. Wan L, Deng C, Chen H, et al. Flame-retarded thermoplastic polyurethane elastomer: from organic materials to nanocomposites and new prospects. *Chem Eng J* 2021; 417: 129314.
26. Rallini M, Natali M, Kenny JM, et al. Effect of boron carbide nanoparticles on the fire reaction and fire resistance of carbon fiber/epoxy composites. *Polymer* 2013; 54(19): 5154–5165.
27. Jubsilp C, Panyawanitchakun C and Rimdusit S. Flammability and thermomechanical properties of dianhydride-modified polybenzoxazine composites reinforced with carbon fiber. *Polym Compos* 2013; 34(12): 2067–2075.
28. Zhang J, Delichatsios M and Colobert M. Assessment of fire dynamics simulator for heat flux and flame heights predictions from fires in SBI tests. *Fire Technol* 2010; 46(2): 291–306.
29. Horrocks A and Kandola BK. Flammability and fire resistance of composites. In: *Design and manufacture of textile composites*. Amsterdam: Elsevier, 2005, pp. 330–363.
30. Kozłowski R and Władysław-Przybylak M. Flammability and fire resistance of composites reinforced by natural fibers. *Polym Adv Technol* 2008; 19(6): 446–453.
31. Bhat T, Chevali V, Liu X, et al. Fire structural resistance of basalt fibre composite. *Compos Appl Sci Manuf* 2015; 71: 107–115.
32. Kim M, Choe J and Lee DG. Development of the fire retardant glass fabric/carbonized phenolic composite. *Compos Struct* 2016; 148: 191–197.
33. Kil H-S and Lee S. High flame retardancy of oxidized polyacrylonitrile fibers prepared by effective plasma-assisted thermal stabilization and electron-beam irradiation. *Compos B Eng* 2019; 178: 107458.
34. Yang H, Gong J, Wen X, et al. Effect of carbon black on improving thermal stability, flame retardancy and electrical conductivity of polypropylene/carbon fiber composites. *Compos Sci Technol* 2015; 113: 31–37.
35. Ghazzawi YM, Osorio AF and Heitzmann MT. Fire performance of continuous glass fibre reinforced polycarbonate composites: the effect of fibre architecture on the fire properties of polycarbonate composites. *J Compos Mater* 2019; 53(12): 1705–1715.
36. Atabek Savas L, Mutlu A, Dike AS, et al. Effect of carbon fiber amount and length on flame retardant and mechanical properties of intumescent polypropylene composites. *J Compos Mater* 2018; 52(4): 519–530.
37. Grigoriou K and Mouritz A. Influence of ply stacking pattern on the structural properties of quasi-isotropic carbon-epoxy laminates in fire. *Compos Appl Sci Manuf* 2017; 99: 113–120.
38. Mouritz AP and Gibson AG. *Fire properties of polymer composite materials*. Dordrecht: Springer Science & Business Media, 2007.
39. Katsoulis C, Kandola BK, Myler P, et al. Post-fire flexural performance of epoxy-nanocomposite matrix glass fibre composites containing conventional flame retardants. *Compos Appl Sci Manuf* 2012; 43(8): 1389–1399.

40. Bazli M and Abolfazli M. Mechanical properties of fibre reinforced polymers under elevated temperatures: an overview. *Polymers* 2020; 12(11): 2600.
41. Anjang A, Mouritz A and Feih S. Influence of fibre orientation on the tensile performance of sandwich composites in fire. *Compos Appl Sci Manuf* 2017; 100: 342–351.
42. Lu Z, Xian G and Li H. Effects of elevated temperatures on the mechanical properties of basalt fibers and BFRP plates. *Construct Build Mater* 2016; 127: 1029–1036.
43. Wang K, Young B and Smith ST. Mechanical properties of pultruded carbon fibre-reinforced polymer (CFRP) plates at elevated temperatures. *Eng Struct* 2011; 33(7): 2154–2161.
44. Salasinska K, Celiński M, Mizera K, et al. Synergistic effect between histidine phosphate complex and hazelnut shell for flammability reduction of low-smoke emission epoxy resin. *Polym Degrad Stabil* 2020; 181: 109292.
45. Huang H, Dong D, Li W, et al. Synergistic effect of MXene on the flame retardancy and thermal degradation of intumescent flame retardant biodegradable poly (lactic acid) composites. *Chin J Chem Eng* 2020; 28(7): 1981–1993.
46. Costes L, Laoutid F, Aguedo M, et al. Phosphorus and nitrogen derivatization as efficient route for improvement of lignin flame retardant action in PLA. *Eur Polym J* 2016; 84: 652–667.
47. Yang H, Song L, Tai Q, et al. Comparative study on the flame retarded efficiency of melamine phosphate, melamine phosphite and melamine hypophosphite on poly (butylene succinate) composites. *Polym Degrad Stabil* 2014; 105: 248–256.
48. Wang B, Li P, Xu YJ, et al. Bio-based, nontoxic and flame-retardant cotton/alginate blended fibres as filling materials: thermal degradation properties, flammability and flame-retardant mechanism. *Compos B Eng* 2020; 194: 108038.
49. Ferry L, Dorez G, Taguet A, et al. Chemical modification of lignin by phosphorus molecules to improve the fire behavior of polybutylene succinate. *Polym Degrad Stabil* 2015; 113: 135–143.
50. Tranchard P, Duquesne S, Samyn F, et al. Kinetic analysis of the thermal decomposition of a carbon fibre-reinforced epoxy resin laminate. *J Anal Appl Pyrol* 2017; 126: 14–21.
51. Fonseca V, Fernandes Jr VJ, Araujo A, et al. Effect of halogenated flame-retardant additives in the pyrolysis and thermal degradation of polyester/sisal composites. *J Therm Anal Calorim* 2005; 79(2): 429–433.
52. Chen X, Huo L, Jiao C, et al. TG–FTIR characterization of volatile compounds from flame retardant polyurethane foams materials. *J Anal Appl Pyrol* 2013; 100: 186–191.
53. Saba N, Jawaid M, Paridah M, et al. A review on flammability of epoxy polymer, cellulosic and non-cellulosic fiber reinforced epoxy composites. *Polym Adv Technol* 2016; 27(5): 577–590.
54. Zhao B, Liang W-J, Wang J-S, et al. Synthesis of a novel bridged-cyclotriphosphazene flame retardant and its application in epoxy resin. *Polym Degrad Stabil* 2016; 133: 162–173.
55. Yang W, Song L and Hu Y. Comparative study on thermal decomposition and combustion behavior of glass-fiber reinforced poly (1, 4-butylene terephthalate) composites containing trivalent metal (Al, La, Ce) hypophosphite. *Polym Compos* 2013; 34(11): 1832–1839.
56. Ferry L, Sonnier R, Lopez-Cuesta J-M, et al. Thermal degradation and flammability of polyamide 11 filled with nano Boehmite. *J Therm Anal Calorim* 2017; 129(2): 1029–1037.

57. Realinho V, Haurie L, Antunes M, et al. Thermal stability and fire behaviour of flame retardant high density rigid foams based on hydromagnesite-filled polypropylene composites. *Compos B Eng* 2014; 58: 553–558.
58. Ogabi R, Manescau B, Chetehouna K, et al. A study of thermal degradation and fire behaviour of polymer composites and their gaseous emission assessment. *Energies* 2021; 14(21): 7070.
59. Langot J, Pelzmann T, Chávez-Gómez P, et al. Multi-physics modeling of the ignition of polymer matrix composites exposed to fire. *Fire Saf J* 2021; 122: 103312.
60. Lyon RE. *Federal aviation administration research in fire safe materials for aircraft interiors*. Diamond Bar, CA: Society for the Advancement of Material and Process Engineering. 1996, pp. 344–350.
61. Sorathia U, Lyon R, Gann R, et al. Materials and fire threat. *SAMPE J* 1996; 32(3): 8–15.
62. Ventriglio DR. Fire safe materials for navy ships. *Nav Eng J* 1982; 94(5): 65–74.
63. Brown JE, Braun E and Twilley WH. *Cone calorimeter evaluation of the flammability of composite materials*. Gaithersburg, MD: US Department of Commerce. 1988.
64. Sorathia U, Dapp T and Kerr J. Flammability characteristics of composites for shipboard and submarine internal applications. *How Concept Becomes Reality* 1991; 36: 1868–1878.
65. Hume J. Assessing the fire performance characteristics of GRP composites. In: Proceedings of the International Conference on Materials & Design Against Fire, London, 27–28 October 1992, pp. 11–15.
66. Tewarson A and Macaione DP. Polymers and composites—an examination of fire spread and generation of heat and fire products. *J Fire Sci* 1993; 11(5): 421–441.
67. Scudamore M. Fire performance studies on glass-reinforced plastic laminates. *Fire Mater* 1994; 18(5): 313–325.
68. Grenier AT, Dembsey NA and Barnett JR. Fire characteristics of cored composite materials for marine use. *Fire Saf J* 1998; 30(2): 137–159.
69. Le Bras M, Bourbigot S, Mortaigne B, et al. Comparative study of the fire behaviour of glass-fibre reinforced unsaturated polyesters using a cone calorimeter. *Polym Polym Compos* 1998; 6(8): 535–539.
70. Mouritz A, Mathys Z and Gibson A. Heat release of polymer composites in fire. *Compos Appl Sci Manuf* 2006; 37(7): 1040–1054.
71. Lyon RE, Demario J, Walters RN, et al. Flammability of glass fiber-reinforced polymer composites. In: Proceedings of the fourth conference on composites in fire, University of Newcastle upon Tyne, 15–16 September 2005.
72. Mouritz A. *Fire safety of advanced composites for aircraft, ATSB research and analysis report*. Canberra: Australian Transport Safety Bureau, 2006.
73. Mouritz A. Review of smoke toxicity of fiber-polymer composites used in aircraft. *J Aircraft* 2009; 46(3): 737–745.
74. Boyd SE, Bausano JV, Case SW, et al. Mechanistic approach to structural fire modeling of composites. *Fire Technol* 2011; 47(4): 941–983.
75. Ritchie SJ, Steckler KD, Hamins A, et al. The effect of sample size on the heat release rate of charring materials. In: Fire Safety Science—Proceedings of the 5th International Symposium. Boston, 3–7 March 1997, pp. 177–188.

76. Potocki ML, Tuttle ME and Mescher AM, Behavior of polymeric composites exposed to a heat flux simulating fire. *ASME International Mechanical Engineering Congress and Exposition* 1998; 16097: 325–332.
77. Chang C. Thermal effects on polymer composite structures. *Theor Appl Fract Mech* 1986; 6(2): 113–120.
78. Mcmanus HL and Springer GS. High temperature thermomechanical behavior of carbon-phenolic and carbon-carbon composites, i. analysis. *J Compos Mater* 1992; 26(2): 206–229.
79. Dao M and Asaro RJ. A study on failure prediction and design criteria for fiber composites under fire degradation. *Compos Appl Sci Manuf* 1999; 30(2): 123–131.
80. Krysl P, Ramroth W, Stewart L, et al. Finite element modelling of fibre reinforced polymer sandwich panels exposed to heat. *Int J Numer Methods Eng* 2004; 61(1): 49–68.
81. Asaro R, Krysl P and Ramroth W. Structural fire integrity of FRP composites: analysis and design. In: *Modeling of naval composite structures in fire*. Melbourne: Acclaim Printing, 2006.
82. Gu P and Asaro R. Wrinkling of sandwich polymer matrix composite panels under transverse thermal gradients. *Fire Saf J* 2008; 43(2): 151–160.
83. Gu P and Asaro R. Designing sandwich polymer matrix composite panels for structural integrity in fire. *Compos Struct* 2009; 88(3): 461–467.
84. Luo C, Xie W and DesJardin P. Numerical simulation of composite structure response from a fire plume. In: *Proceedings of the SAMPE 2005 symposium & exhibition, Long Beach*.
85. Luo C, Xie W and DesJardin PE. Fluid-structure simulations of composite material response for fire environments. *Fire Technol* 2011; 47(4): 887–912.
86. Lua J and O'Brien J. Fire simulation for woven fabric composites with temperature and mass dependent thermal-mechanical properties. *Proceeding of composites in fire* 2003; 3.
87. Gibson AG, Wu Y-S, Evans JT, et al. Laminate theory analysis of composites under load in fire. *J Compos Mater* 2006; 40(7): 639–658.
88. Feih S, Mathys Z, Gibson A, et al. Modelling the tension and compression strengths of polymer laminates in fire. *Compos Sci Technol* 2007; 67(3–4): 551–564.
89. Feih S, Mathys Z, Gibson A, et al. Modelling the compression strength of polymer laminates in fire. *Compos Appl Sci Manuf* 2007; 38(11): 2354–2365.
90. Easby R, Feih S, Konstantis C, et al. Failure model for phenolic and polyester pultrusions under load in fire. *Plast, Rubber Compos* 2007; 36(9): 379–388.
91. Toubia E, Morgan A and Elmushyakh A. Post-fire residual mechanical properties of a composite laminate—experimental study. In: *CAMX 2017-The Composites and Advanced Materials Expo, Orlando*, pp. 11–14.
92. Mathys Z, Gardiner C, Mouritz A, et al. Mechanical properties of GRP composites with localised thermal damage. *Int J Mater Prod Technol* 2002; 17(1–2): 134–142.
93. Gardiner C, Mathys Z and Mouritz A. Post-fire structural properties of burnt GRP plates. *Mar Struct* 2004; 17(1): 53–73.
94. Mouritz A, Mathys Z and Gardiner C. Thermomechanical modelling the fire properties of fibre-polymer composites. *Compos B Eng* 2004; 35(6–8): 467–474.
95. Mouritz A and Gardiner C. Compression properties of fire-damaged polymer sandwich composites. *Composites* 2002; 33: 609–620.

96. Dutta S, Das R and Bhattacharyya D. A multi-physics framework model towards coupled fire-structure interaction for Flax/PP composite beams. *Compos B Eng* 2019; 157: 207–218.
97. Pacheco-Blazquez R, Di Capua D, García-Espinosa J, et al. Thermo-mechanical analysis of laminated composites shells exposed to fire. *Eng Struct* 2022; 253: 113679.
98. Henderson JB, Wiebelt JA and Tant M. A model for the thermal response of polymer composite materials with experimental verification. *J Compos Mater* 1985; 19(6): 579–595.
99. Gao Y and Oterkus S. Coupled thermo-fluid-mechanical peridynamic model for analysing composite under fire scenarios. *Compos Struct* 2021; 255: 113006.
100. Luo C, Lua J and DesJardin PE. Thermo-mechanical damage modeling of polymer matrix sandwich composites in fire. *Compos Appl Sci Manuf* 2012; 43(5): 814–821.
101. Bhat T, Kandare E, Gibson A, et al. Compressive softening and failure of basalt fibre composites in fire: modelling and experimentation. *Compos Struct* 2017; 165: 15–24.
102. Hurley MJ, Gottuk D, Hall JR, et al. *SFPE handbook of fire protection engineering*. New York: Springer, 2015.
103. Li H, Ning N, Zhang L, et al. Different flame retardancy effects and mechanisms of aluminium phosphinate in PPO, TPU and PP. *Polym Degrad Stabil* 2014; 105: 86–95.
104. Shao N, Qu Y, Hou L, et al. Effect of starch-based flame retardant on the thermal degradation and combustion properties of reconstituted tobacco sheet. *Cellulose* 2021; 28(2): 741–755.
105. Fina A, Bocchini S and Camino G. Catalytic fire retardant nanocomposites. *Polym Degrad Stabil* 2008; 93(9): 1647–1655.
106. Grange N, Chetehouna K, Gascoin N, et al. Numerical investigation of the heat transfer in an aeronautical composite material under fire stress. *Fire Saf J* 2016; 80: 56–63.
107. Timme S, Trappe V, Korzen M, et al. Fire stability of carbon fiber reinforced polymer shells on the intermediate-scale. *Compos Struct* 2017; 178: 320–329.
108. Fateh T, Kahanji C, Joseph P, et al. A study of the effect of thickness on the thermal degradation and flammability characteristics of some composite materials using a cone calorimeter. *J Fire Sci* 2017; 35(6): 547–564.
109. Didane N, Giraud S, Devaux E, et al. A comparative study of POSS as synergists with zinc phosphinates for PET fire retardancy. *Polym Degrad Stabil* 2012; 97(3): 383–391.
110. Yang W, Tang G, Song L, et al. Effect of rare earth hypophosphite and melamine cyanurate on fire performance of glass-fiber reinforced poly (1, 4-butylene terephthalate) composites. *Thermochim Acta* 2011; 526(1–2): 185–191.
111. Zhao B, Liu Y-T, Zhang C-Y, et al. A novel phosphoramidate and its application on cotton fabrics: synthesis, flammability and thermal degradation. *J Anal Appl Pyrol* 2017; 125: 109–116.
112. Seefeldt H and Braun U. A new flame retardant for wood materials tested in wood-plastic composites. *Macromol Mater Eng* 2012; 297(8): 814–820.
113. Wen Y, Cheng Z, Li W, et al. A novel oligomer containing DOPO and ferrocene groups: synthesis, characterization, and its application in fire retardant epoxy resin. *Polym Degrad Stabil* 2018; 156: 111–124.
114. Marquis DM, Hermouet F and Guillaume É. Effects of reduced oxygen environment on the reaction to fire of a poly (urethane-isocyanurate) foam. *Fire Mater* 2017; 41(3): 245–274.
115. Zhao B, Liu D-Y, Liang W-J, et al. Bi-phase flame-retardant actions of water-blown rigid polyurethane foam containing diethyl-N, N-bis (2-hydroxyethyl) phosphoramidate and expandable graphite. *J Anal Appl Pyrol* 2017; 124: 247–255.

116. Chen X, Feng X and Jiao C. Combustion and thermal degradation properties of flame-retardant TPU based on EMIMPF₆. *J Therm Anal Calorim* 2017; 129(2): 851–857.
117. Ngan A, Jia CQ and Tong S-T. Production, characterization and alternative applications of biochar. In: *Production of Materials from Sustainable Biomass Resources*. Singapore: Springer, 2019, pp. 117–151.
118. Nartey OD and Zhao B. Biochar preparation, characterization, and adsorptive capacity and its effect on bioavailability of contaminants: an overview. *Adv Mater Sci Eng* 2014; 2014: 1–12.
119. Riahipour R, Alizadeh Sahraei A, van de Werken N, et al. Improving flame-retardant, thermal, and mechanical properties of an epoxy using halogen-free fillers. *Sci Eng Compos Mater* 2018; 25(5): 939–946.
120. Wilkie CA and Morgan AB. *Fire retardancy of polymeric materials*. Boca Raton, FL: CRC Press, 2009.
121. Andrew JJ, Arumugam V and Dhakal HN. Effect of intra-ply hybrid patches and hydro-thermal aging on local bending response of repaired GFRP composite laminates. *Molecules* 2020; 25(10): 2325.
122. Short G, Guild F and Pavier M. The effect of delamination geometry on the compressive failure of composite laminates. *Compos Sci Technol* 2001; 61(14): 2075–2086.
123. Chandrasekaran S, Sato N, Tölle F, et al. Fracture toughness and failure mechanism of graphene based epoxy composites. *Compos Sci Technol* 2014; 97: 90–99.
124. Sonnenfeld C, Mendil-Jakani H, Agogué R, et al. Thermoplastic/thermoset multilayer composites: a way to improve the impact damage tolerance of thermosetting resin matrix composites. *Compos Struct* 2017; 171: 298–305.
125. Vu-Khanh T and Denault J. Toughness of reinforced ductile thermoplastics. *J Compos Mater* 1992; 26(15): 2262–2277.
126. Ropers S. Bending behavior of thermoplastic composite sheets. *J Bending Behavior of Thermoplastic Composite* 2017.
127. Sultana N, Hasan M, Habib A, et al. Short jute fiber preform reinforced polypropylene thermoplastic composite: experimental investigation and its theoretical stiffness prediction. *ACS Omega* 2023; 8(27): 24311–24322.
128. Saleem H, Edathil A, Ncube T, et al. Mechanical and thermal properties of thermoset-graphene nanocomposites. *Macromol Mater Eng* 2016; 301(3): 231–259.
129. Ersoy N, Garstka T, Potter K, et al. Development of the properties of a carbon fibre reinforced thermosetting composite through cure. *J Composites Part A: Applied Science Manufacturing* 2010; 41(3): 401–409.
130. Pilato LA and Michno MJ. *Advanced composite materials*. Heidelberg: Springer Science & Business Media, 1994.
131. Yaashikaa P, Kumar PS, Varjani S, et al. A critical review on the biochar production techniques, characterization, stability and applications for circular bioeconomy. *Biotechnol Rep* 2020; 28: e00570.
132. Xing W, Jie G, Song L, et al. Flame retardancy and thermal properties of epoxy acrylate resin/alpha-zirconium phosphate nanocomposites used for UV-curing flame retardant films. *Mater Chem Phys* 2011; 125(1–2): 196–201.
133. Zhou S, Ning M, Xu Y, et al. Effects of melamine phosphate on the thermal decomposition and combustion behavior of reconstituted tobacco sheet. *J Therm Anal Calorim* 2013; 112(3): 1269–1276.

134. Xiao F, Wu K, Luo F, et al. Influence of ionic liquid-based metal–organic hybrid on thermal degradation, flame retardancy, and smoke suppression properties of epoxy resin composites. *J Mater Sci* 2018; 53(14): 10135–10146.
135. Rashid M, Chetehouna K, Cablé A, et al. Analysing flammability characteristics of green biocomposites: an overview. *Fire Technol* 2021; 57(1): 31–67.
136. Li B. Influence of polymer additives on thermal decomposition and smoke emission of poly (vinyl chloride). *Polym Degrad Stabil* 2003; 82(3): 467–476.
137. Zhang W, Li X, Guo X, et al. Mechanical and thermal properties and flame retardancy of phosphorus-containing polyhedral oligomeric silsesquioxane (DOPO-POSS)/polycarbonate composites. *Polym Degrad Stabil* 2010; 95(12): 2541–2546.
138. Ren Y, Wang Y, Wang L, et al. Evaluation of intumescent fire retardants and synergistic agents for use in wood flour/recycled polypropylene composites. *Construct Build Mater* 2015; 76: 273–278.
139. Zhang W, Li X and Yang R. Flame retardancy mechanisms of phosphorus-containing polyhedral oligomeric silsesquioxane (DOPO-POSS) in polycarbonate/acrylonitrile-butadiene-styrene blends. *Polym Adv Technol* 2012; 23(3): 588–595.
140. Jiao C, Wang H, Chen X, et al. Flame retardant and thermal degradation properties of flame retardant thermoplastic polyurethane based on HGM@[EOOEMIm] [BF₄]. *J Therm Anal Calorim* 2019; 135(6): 3141–3152.
141. Müller P and Schartel B. Melamine poly (metal phosphates) as flame retardant in epoxy resin: performance, modes of action, and synergy. *J Appl Polym Sci* 2016; 133(24).
142. Nistor M-T and Vasile C. Influence of the nanoparticle type on the thermal decomposition of the green starch/poly (vinyl alcohol)/montmorillonite nanocomposites. *J Therm Anal Calorim* 2013; 111(3): 1903–1919.
143. Shi Z, Fu R, Agathopoulos S, et al. Thermal conductivity and fire resistance of epoxy molding compounds filled with Si₃N₄ and Al (OH) ₃. *Mater Des* 2012; 34: 820–824.
144. Patrick Lim W, Mariatti M, Chow W, et al. Effect of intumescent ammonium polyphosphate (APP) and melamine cyanurate (MC) on the properties of epoxy/glass fiber composites. *Compos B Eng* 2012; 43(2): 124–128.
145. Wang L, Sanchez-Soto M and Maspoch ML. Polymer/clay aerogel composites with flame retardant agents: mechanical, thermal and fire behavior. *Mater Des (1980-2015)* 2013; 52: 609–614.
146. Ogrodowska K, Łuszcz K and Garbacz A. Nanomodification, hybridization and temperature impact on shear strength of basalt fiber-reinforced polymer bars. *Polymers* 2021; 13(16): 2585.
147. Zhi M, Liu Q, Chen H, et al. Thermal stability and flame retardancy properties of epoxy resin modified with functionalized graphene oxide containing phosphorus and silicon elements. *ACS Omega* 2019; 4(6): 10975–10984.
148. Ochi M, Takahashi R and Terauchi A. Phase structure and mechanical and adhesion properties of epoxy/silica hybrids. *Polymer* 2001; 42(12): 5151–5158.
149. Liu Y-L, Hsu C-Y, Wei W-L, et al. Preparation and thermal properties of epoxy-silica nanocomposites from nanoscale colloidal silica. *Polymer* 2003; 44(18): 5159–5167.

150. Vu CM and Bach Q-V. Effects of DOPO-grafted epoxidized soybean oil on fracture toughness and flame retardant of epoxy resin/rice husk silica hybrid. *Macromol Res* 2020; 28(9): 826–834.
151. Wang K, Liu H, Wang C, et al. Flame-retardant performance of epoxy resin composites with SiO₂ nanoparticles and phenethyl-bridged DOPO derivative. *ACS Omega* 2021; 6(1): 666–674.
152. Liu S, Yan H, Fang Z, et al. Effect of graphene nanosheets on morphology, thermal stability and flame retardancy of epoxy resin. *Compos Sci Technol* 2014; 90: 40–47.
153. Yu B, Shi Y, Yuan B, et al. Enhanced thermal and flame retardant properties of flame-retardant-wrapped graphene/epoxy resin nanocomposites. *J Mater Chem A Mater* 2015; 3(15): 8034–8044.
154. Zhang XH, Liu F, Chen S, et al. Novel flame retardant thermosets from nitrogen-containing and phosphorus-containing epoxy resins cured with dicyandiamide. *J Appl Polym Sci* 2007; 106(4): 2391–2397.
155. Guo Y, Bao C, Song L, et al. In situ polymerization of graphene, graphite oxide, and functionalized graphite oxide into epoxy resin and comparison study of on-the-flame behavior. *Ind Eng Chem Res* 2011; 50(13): 7772–7783.
156. Sandler J, Shaffer M, Prasse T, et al. Development of a dispersion process for carbon nanotubes in an epoxy matrix and the resulting electrical properties. *Polymer* 1999; 40(21): 5967–5971.
157. Peeterbroeck S, Laoutid F, Taulemesse J, et al. Mechanical properties and flame-retardant behavior of ethylene vinyl acetate/high-density polyethylene coated carbon nanotube nanocomposites. *Adv Funct Mater* 2007; 17(15): 2787–2791.
158. Kashiwagi T, Mu M, Winey K, et al. Relation between the viscoelastic and flammability properties of polymer nanocomposites. *Polymer* 2008; 49(20): 4358–4368.
159. Kashiwagi T, Grulke E, Hilding J, et al. Thermal and flammability properties of polypropylene/carbon nanotube nanocomposites. *Polymer* 2004; 45(12): 4227–4239.
160. Schartel B, Pötschke P, Knoll U, et al. Fire behaviour of polyamide 6/multiwall carbon nanotube nanocomposites. *Eur Polym J* 2005; 41(5): 1061–1070.
161. Laoutid F, Bonnaud L, Alexandre M, et al. New prospects in flame retardant polymer materials: from fundamentals to nanocomposites. *Mater Sci Eng R Rep* 2009; 63(3): 100–125.
162. Tseng C-H, Wang C-C and Chen C-Y. Functionalizing carbon nanotubes by plasma modification for the preparation of covalent-integrated epoxy composites. *Chem Mater* 2007; 19(2): 308–315.
163. Gao L, Chou T-W, Thostenson ET, et al. Highly conductive polymer composites based on controlled agglomeration of carbon nanotubes. *Carbon* 2010; 48(9): 2649–2651.
164. Gong S, Zhu Z and Meguid S. Carbon nanotube agglomeration effect on piezoresistivity of polymer nanocomposites. *Polymer* 2014; 55(21): 5488–5499.
165. Manchado ML, Valentini L, Biagiotti J, et al. Thermal and mechanical properties of single-walled carbon nanotubes–polypropylene composites prepared by melt processing. *Carbon* 2005; 43(7): 1499–1505.
166. Jam J, Asghar A and Omidvar N. Local aggregation effect of carbon nanotubes on the elastic property of carbon nanotube reinforced composites. *J Comput Theor Nanosci* 2014; 11(1): 102–109.

167. Cui L-J, Wang YB, Xiu WJ, et al. Effect of functionalization of multi-walled carbon nanotube on the curing behavior and mechanical property of multi-walled carbon nanotube/epoxy composites. *Mater Des* 2013; 49: 279–284.
168. Zhu J, Kim J, Peng H, et al. Improving the dispersion and integration of single-walled carbon nanotubes in epoxy composites through functionalization. *Nano Lett* 2003; 3(8): 1107–1113.
169. Romanov VS, Lomov SV, Verpoest I, et al. Stress magnification due to carbon nanotube agglomeration in composites. *Compos Struct* 2015; 133: 246–256.
170. Rallini M, Natali M, Monti M, et al. Effect of alumina nanoparticles on the thermal properties of carbon fibre-reinforced composites. *Fire and materials* 2014; 38(3): 339–355.
171. George P, Bhowmik S, Abraham M, et al. High-performance fire-resistant polymeric nanocomposite for aerospace applications. *Proc Inst Mech Eng Part L* 2019; 233(2): 97–108.
172. Guo Y, Xue Y, Zuo X, et al. Capitalizing on the molybdenum disulfide/graphene synergy to produce mechanical enhanced flame retardant ethylene-vinyl acetate composites with low aluminum hydroxide loading. *Polym Degrad Stabil* 2017; 144: 155–166.
173. Qin Z, Li D, Li Q, et al. Effect of nano-aluminum hydroxide on mechanical properties, flame retardancy and combustion behavior of intumescent flame retarded polypropylene. *Mater Des* 2016; 89: 988–995.
174. Wang M, Zeng X-F, Chen J-Y, et al. Magnesium hydroxide nanodispersion for polypropylene nanocomposites with high transparency and excellent fire-retardant properties. *Polym Degrad Stabil* 2017; 146: 327–333.
175. Kingston C, Zepp R, Andrady A, et al. Release characteristics of selected carbon nanotube polymer composites. *Carbon* 2014; 68: 33–57.
176. Bikiaris D. Can nanoparticles really enhance thermal stability of polymers? Part II: an overview on thermal decomposition of polycondensation polymers. *Thermochim Acta* 2011; 523(1–2): 25–45.
177. Niu L, Xu J, Yang W, et al. Research on nano-Sb₂O₃ flame retardant in char formation of PBT. *Ferroelectrics* 2018; 523(1): 14–21.
178. Shi Y, Liu C, Duan Z, et al. Interface engineering of MXene towards super-tough and strong polymer nanocomposites with high ductility and excellent fire safety. *Chem Eng J* 2020; 399: 125829.
179. Lee J-H, Zhang W, Ryu H-J, et al. Enhanced thermal stability and mechanical property of EVA nanocomposites upon addition of organo-intercalated LDH nanoparticles. *Polymer* 2019; 177: 274–281.
180. Swolfs Y, Verpoest I and Gorbatiikh L. Recent advances in fibre-hybrid composites: materials selection, opportunities and applications. *Int Mater Rev* 2019; 64(4): 181–215.
181. Sarasini F, Tirillò J, Valente M, et al. Hybrid composites based on aramid and basalt woven fabrics: impact damage modes and residual flexural properties. *Mater Des* 2013; 49: 290–302.
182. Dalfi HK, Al-Obaidi A, Selver E, et al. Influence of yarn-hybridisation on the mechanical performance and thermal conductivity of composite laminates. *Journal of Industrial Textiles* 2022; 51(3_suppl): 5086S–5112S.
183. Swolfs Y, Gorbatiikh L and Verpoest I. Fibre hybridisation in polymer composites: a review. *Compos Appl Sci Manuf* 2014; 67: 181–200.
184. Kretsis G. A review of the tensile, compressive, flexural and shear properties of hybrid fibre-reinforced plastics. *Composites* 1987; 18(1): 13–23.

185. Yu H, Longana ML, Jalalvand M, et al. Pseudo-ductility in intermingled carbon/glass hybrid composites with highly aligned discontinuous fibres. *Compos Appl Sci Manuf* 2015; 73: 35–44.
186. Dalfi H, Katnam KB and Potluri P. Intra-laminar toughening mechanisms to enhance impact damage tolerance of 2D woven composite laminates via yarn-level fiber hybridization and fiber architecture. *Polym Compos* 2019; 40(12): 4573–4587.
187. Dalfi H, Babu-Katnum K, Potluri P, et al. The role of hybridisation and fibre architecture on the post-impact flexural behaviour of composite laminates. *J Compos Mater* 2021; 55(11): 1499–1515.
188. Dalfi H. Effect of intra-yarn hybridisation and fibre architecture on the impact response of composite laminates: experimental and numerical analysis. *Proc IME C J Mech Eng Sci* 2021: 09544062211037363.
189. Dalfi H. Improving the mechanical performance and impact damage tolerance of glass composite laminates via multi-scales of hybridisation. *Proceedings of the Institution of Mechanical Engineers Part L Journal of Materials Design and Applications* 2022; 236(12): 2339–2356.
190. Dalfi H. Effect of intra-yarn hybridisation and fibre architecture on the impact response of composite laminates: experimental and numerical analysis. *Proceedings of the Institution of Mechanical Engineers Part L Journal of Materials Design and Applications* 2022; 236(6): 3004–3026.
191. Dalfi H, Al-Obaidi AJ and Razaq HJSP. The influence of the inter-ply hybridisation on the mechanical performance of composite laminates: experimental and numerical analysis. *Sci Prog* 2021; 104(2): 00368504211023285.
192. Zuhudi NZM, Lin RJ and Jayaraman K. Flammability, thermal and dynamic mechanical properties of bamboo–glass hybrid composites. *J Thermoplast Compos Mater* 2016; 29(9): 1210–1228.
193. Rao S, Bhardwaj A, Beehag A, et al. Fire performance of flax laminates and their hybrids. *Adv Mater Res* 2012; 410: 114–117.
194. Rashid MR and Kandola B. Effect of reinforcing elements on burning behavior of fiber-reinforced polymeric composites. *AATCC Rev* 2010; 10(4).
195. Chae HG and Kumar S. Rigid-rod polymeric fibers. *J Appl Polym Sci* 2006; 100(1): 791–802.
196. Kelly A and Zweben CH. *Comprehensive composite materials*. Amsterdam: Elsevier, 2000.
197. Kim M, Choe J and Lee DG. Development of the fire-retardant sandwich structure using an aramid/glass hybrid composite and a phenolic foam-filled honeycomb. *Compos Struct* 2016; 158: 227–234.
198. Cong X, Khalili P, Zhu C, et al. Investigation of fire protection performance and mechanical properties of thin-ply bio-epoxy composites. *Polymers* 2021; 13(5): 731.
199. Abdul Khalil H, Bhat I, Jawaid M, et al. Bamboo fibre reinforced biocomposites: a review. *Mater Des* 2012; 42: 353–368.
200. Christke S, Gibson A, Grigoriou K, et al. Multi-layer polymer metal laminates for the fire protection of lightweight structures. *Mater Des* 2016; 97: 349–356.
201. Yang X, Zhan L, Peng Y, et al. Interface controlled micro-and macro-mechanical properties of vibration processed carbon fiber/epoxy composites. *Polymers* 2021; 13(16): 2764.

202. Shi X-H, Chen L, Zhao Q, et al. Epoxy resin composites reinforced and fire-retarded by surficially-treated carbon fibers via a tunable and facile process. *Compos Sci Technol* 2020; 187: 107945.
203. Jiang J, Cheng Y, Liu Y, et al. Intergrowth charring for flame-retardant glass fabric-reinforced epoxy resin composites. *J Mater Chem A Mater* 2015; 3(8): 4284–4290.
204. Wu K, Wang X, Xu Y, et al. Flame retardant efficiency of modified para-aramid fiber synergizing with ammonium polyphosphate on PP/EPDM. *Polym Degrad Stabil* 2020; 172: 109065.
205. Du S-l., Lin X-b., Jian R-k., et al. Flame-retardant wrapped ramie fibers towards suppressing “candlewick effect” of polypropylene/ramie fiber composites. *Chin J Polym Sci* 2015; 33(1): 84–94.
206. Liu L, Liu Y, Han Y, et al. Interfacial charring method to overcome the wicking action in glass fiber-reinforced polypropylene composite. *Compos Sci Technol* 2015; 121: 9–15.
207. Han Y, Xu Y, Liu Y, et al. An efficient interfacial flame-resistance mode to prepare glass fiber reinforced and flame retarded polyamide 6 with high performance. *J Mater Chem A Mater* 2013; 1(35): 10228–10233.
208. Chen W, Liu P, Liu Y, et al. Interfacial carbonation for efficient flame retardance of glass fiber-reinforced polyamide 6. *Polym Chem* 2015; 6(24): 4409–4414.
209. Shi X-H, Xu YJ, Long JW, et al. Layer-by-layer assembled flame-retardant architecture toward high-performance carbon fiber composite. *Chem Eng J* 2018; 353: 550–558.
210. Shi X-H, Chen L, Liu B-W, et al. Carbon fibers decorated by polyelectrolyte complexes toward their epoxy resin composites with high fire safety. *Chin J Polym Sci* 2018; 36(12): 1375–1384.
211. Araby S, Philips B, Meng Q, et al. Recent advances in carbon-based nanomaterials for flame retardant polymers and composites. *Composites Part B: Engineering* 2021; 212: 108675.