

# A review of interconnection technologies for improved crystalline silicon solar cell photovoltaic module assembly

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## Abstract

The identification, adoption and utilisation of reliable interconnection technology to assembly crystalline silicon solar cells in photovoltaic (PV) module are critical to ensure that the device performs continually up to 20 years of its design life span. With report that 40.7 % of this type of PV module fails at interconnection coupled with recent reports of increase in such failure in the tropics, the review of interconnection technologies employed in crystalline silicon solar cells manufacture has become imperative. Such review is capable of providing information that can improve the reliability of the system when adopted which in turn will increase silicon PV module production share more than the current value of 90.956%. This review presents the characteristics of interconnect contacts in conventional cells and other unconventional crystalline silicon cells. It compares series resistance, shadowing losses and the induced thermo-mechanical stress in the interconnection for each interconnection technique employed. The paper also reviews interconnection technologies in these assemblies and presents a comparison of their concept, cell type, joint type, manufacturing techniques and production status. Moreover, the study reviews and discusses the material and technological reliability challenges of silicon solar cells interconnection. The review identifies laser soldering technology as one which has the potential of making interconnection with higher reliability when compared with conventional soldering technology. It was found that this technology supports the current design trend of thinner, wider and cheaper crystalline silicon solar cells significantly whilst producing interconnection that experience relatively lower induced thermo-mechanical stress. The authors recommend that wider acceptance and usage of laser soldering technology could improve the performance and consequently extend the mean-time-to-failure (MTTF) of photovoltaic modules in general and particularly the ones which operates in the tropics. This will enable improvement in the reliability of PV modules for sustainable energy generation.

**Keywords:** *Photovoltaic modules; Crystalline silicon solar cells; Interconnection technology; Reliability*

## 1. Introduction

Photovoltaic (PV) modules constitute significant development in the worldwide green energy sector in the current campaign to increase sustainable energy production. Currently, the module is in huge demand because they are now used to supply electrical power [1, 2] to many applications. To meet the demand, the production of solar cells has increased because the modules are assembled by interconnecting solar cells to each other. It is expected that in the year 2020, the world annual production of solar cells will be around 100 GW<sub>p</sub> (W<sub>p</sub>, is peak power produced under standard test conditions). While this amount of sustainable power

47 production seems substantial, the continued operation of the module up to its design service  
48 life has become a concern because the desired power generation is lower than expected.

49 The silicon solar cells have been identified as the most viable option suitable for large  
50 volume production [3]. However, it has been reported that the continual generation of  
51 electricity by PV modules, manufactured using this type of cell, in the field for a minimum  
52 life span of 20 years has been a concern [1, 4-6]. One of the key challenges is untimely  
53 failure of solar cells interconnection in the modules [7]. The interconnections provide  
54 electrical, mechanical and thermal contact between the solar semiconductor cell and  
55 electrodes.

56 The failure of the interconnection is caused by degradation of solder joints during module's  
57 field operations due to temperature cycling. Extreme degradation often culminates in module  
58 failure. The existence of this phenomenon and the need to provide solution has been reported  
59 in [1, 6, 8-10]. The analysis of the failure mechanisms of PV modules in the field  
60 demonstrates that the modules fail by many different modes. McCluskey [7] and Campeau, et  
61 al [11] have reported that according to a BP study, 40.7% of PV module failures observed  
62 were due to cell or interconnect breakage. This finding, in addition to other similar findings,  
63 has identified the reliability of PV interconnections as the current challenge in PV modules  
64 manufacture.

65 Consequently, the interconnection technologies of silicon PV modules were selected for  
66 review. Silicon PV modules were chosen because the production of silicon-based solar cells  
67 was 90% of all solar cells produced globally in 2008 [3]. This production share may have  
68 been achieved because Silicon, being the second most abundantly available element on earth  
69 [12], has been used as the primary feedstock. For instance, this largest share of production  
70 was more than 90.956% of global PV module production in 2013 [13] and this share of  
71 production is expected to remain for a long time. This paper explores and characterises  
72 silicon solar cell interconnection technologies used in the various crystalline silicon solar cell  
73 manufactures.

74 The objectives of this study are to present an overview of crystalline silicon PV modules  
75 while dwelling on the characterisation of the solar cell contact and interconnection  
76 technologies. The work advances to seek to review the current reliability challenges of the  
77 interconnection of the solar cells with regards to interconnection technique. In addition, the  
78 paper reviews research trends in solar cell interconnection and assembly technologies -  
79 focusing on the identification of suitable technology to meet long-term reliability demand of  
80 PV modules for energy generation.

81

## 82 **2. Crystalline silicon solar cells interconnection technologies**

83 The contact and interconnection technology of conventional wafer-based silicon solar cells  
84 are discussed in sub-section 2.1 while challenges of conventional interconnection technology  
85 are presented in sub-section 2.2. A comparison of conventional and unconventional  
86 interconnection technologies is discussed in sub-section 2.3.

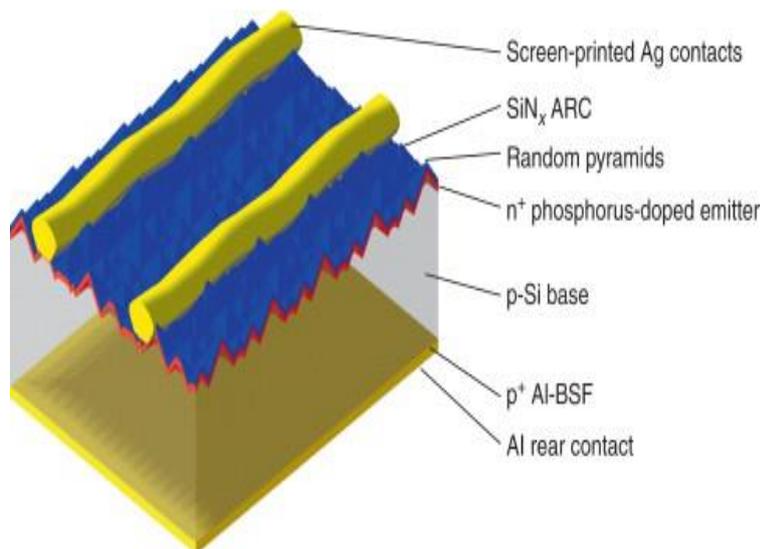
### 87 **2.1 Interconnection technology of conventional crystalline silicon solar cells**

88

89 The assembly and manufacturing process of conventional solar cells involves converting  
90 silicon wafers into solar cells through depositing layers of emitter material and anti-reflection

91 coating (ARC). This process is followed by printing front metal electrode and back contacts  
92 on the cell material as well as soldering of highly conductive solder-coated ribbon strip along  
93 the length of the cell. An extended part of the ribbon strip is soldered to the back of a  
94 neighbouring cell to enable current transfer from the front of one cell to the back of a  
95 neighbouring cell in a series connection [5]. The use of low resistant electrode and finer lines  
96 for a larger aperture in the manufacture enables the delivery of higher short circuit current  
97 ( $I_{sc}$ ) and fill factor to the ribbon strip [14]. The interconnection of solar cells in crystalline  
98 silicon modules by soldering process is a high temperature process which occurs at about 250  
99 °C. The elevated temperature soldering induces thermo-mechanical stress in the solder joints.

100  
101 Metallization technologies in use for solar cells contact formation include: screen printing,  
102 stencil-printing, pad-printing, ink-jet printing, dispensing technology, photolithographic and  
103 evaporation process, laser micro-sintering, plating (Nickel) and thickening of metal contacts  
104 by means of plating [15]. In the photovoltaic industry, the predominant technique used for the  
105 establishment of an ohmic contact to an n-type emitter of a crystalline silicon solar cell is  
106 screen printing of an Ag-based thick-film paste and firing through the ARC layer [15-18]. A  
107 typical structure of Aluminium Back Surface Field (Al-BSF) solar cell is shown in Fig.1.



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111 Fig.1. Typical structure of Al-BSF solar cell [16]  
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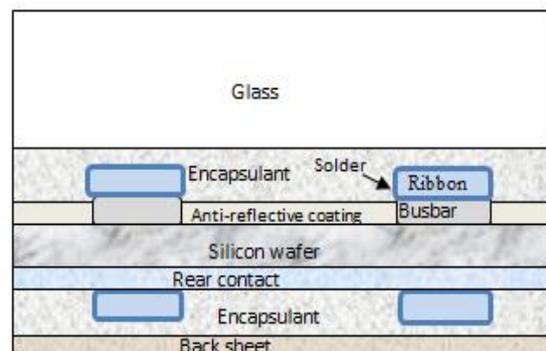
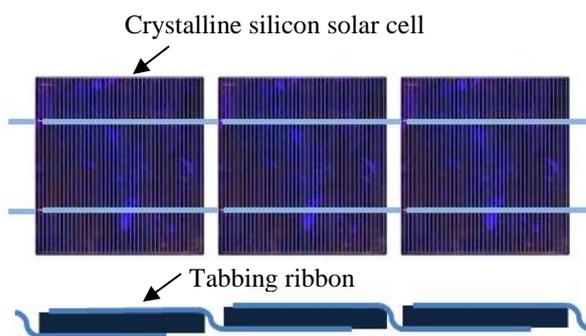
## 114 2.2 Challenges of conventional interconnection technology 115

116 The manufacture of crystalline silicon solar cells using the conventional form of assembly  
117 results in associated challenges which limit the quantity of energy generated as well as  
118 imparts the thermo-mechanical reliability of PV modules. These challenges include series  
119 resistance, shadowing losses and induced thermo-mechanical stress in the solar cells.

120  
121 Series resistance losses are one of the major challenges associated with the manufacture of  
122 solar cells in the conventional form. These losses are created due to metallization for contact  
123 formation and the subsequent tabbing for current collection. In order to reduce these losses,  
124 new concepts are being developed with additional objectives of providing contacts for thinner  
125 wafers. This objective is aimed at: reducing material cost, ensuring low-stress interconnection  
126 between cells and enabling the ease of modules manufacture [19].

127 Another key challenge of conventional interconnection technology is shadowing losses.  
 128 When cells are made wider, thicker interconnection ribbon is required to conduct larger  
 129 currents. It is reported in [20] that increase in the width of interconnection ribbon cross-  
 130 section increases the shadowing losses proportionally. The thickness of ribbon strip is limited  
 131 by built-up stresses in the soldered joint. The differences in coefficient of thermal expansion  
 132 between ribbon interconnection materials and silicon account for this stress accumulation [20,  
 133 21]. Furthermore, stress occurrence at the edge of the wafers due to bending of the  
 134 interconnection ribbon strip which connects the front side with the rear of the neighbouring  
 135 wafer [21] impacts the reliability of the assembly. This situation entails that conventional  
 136 interconnection technology makes a compromise between width and thickness of ribbon strip.  
 137 Apart from shadowing losses, there are also recombination losses which are not influenced by  
 138 interconnection technologies. However, reduction of these losses is desirable to enhance solar  
 139 cell efficiency. This reduction can be achieved through the use of Laser-Fired Contact (LFC)  
 140 process, particularly for the rear surface, to fabricate solar cells with a high quality rear  
 141 surface [15, 22].

142 Induced thermo-mechanical stress in the solar cells is another challenge associated with the  
 143 manufacture of solar cells in the conventional form. The manufacturing process of  
 144 interconnecting wafer-based silicon solar cells involves the use of infra-red (IR) reflow  
 145 soldering. The soldering process consists of two phases. These are stringing or tabbing as  
 146 well as bussing. The former involves the interconnection of solar cells with each other to  
 147 form strings while the later deals with the assembly of the strings of solar cells to form PV  
 148 module [23, 24]. However, this interconnection procedure is difficult and the IR soldering  
 149 induces high mechanical stress in the solder joint which accelerates fatigue related damage.  
 150 Eventually, module failure occurs during field operations thereby halting energy generation.  
 151 Figure 2 presents a diagram of solder interconnection between tabbing ribbon and  
 152 conventional wafer-based crystalline silicon (c-Si) solar cells while Fig. 3 depicts a schematic  
 153 of a typical laminated crystalline Si solar cell showing its cross-section. Figure 4 shows  
 154 typical interconnected solar cells with tabbing and bussing ribbons while Fig. 5 shows a  
 155 typical PV module with complete interconnected solar cells.



156  
 157 Fig. 2. Crystalline silicon solar cells interconnected  
 158 in series with tabbing ribbon

Fig. 3. Schematic of cross-section of a typical laminated crystalline Si solar cell.



Fig. 4. Interconnected solar cells with tabbing and bussing ribbons [25]



Fig. 5. PV Module with complete interconnected solar cells [23]

In order to address some of the challenges of crystalline silicon solar cells interconnection using IR soldering, laser soldering technology is used because it offers some advantages. Laser soldering is well controlled and enables selective processing. Additionally, when used for spot soldering, it delivers heat very fast, precisely and efficiently on a small area of the solder interconnection without making physical contact with the brittle crystalline silicon solar cells. Since physical contact during soldering can result in cell breakage, laser soldering has demonstrated potentials of inducing minimal thermo-mechanical stresses on the solder joint as well as less probability of causing cell breakage during manufacture which will increase production yield [26].

### 2.3 Comparison of different interconnection technologies

In order to address the interconnection challenges, many unconventional PV modules with improved interconnection have been developed. Their interconnect concepts include back contact cells technology. In this technique, the interconnection materials and circuitry are located exclusively behind the cells. Examples include emitter wrap-through (EWT), metallisation wrap-through (MWT) and back-junction back-contact (BJBC). Other cell/module concepts are alternate p- and n-type, honeycomb design (HD), pin up modules (PUM), sliver, spherical and cells with flexible electrode wire grid (Day4 Electrode).

Back contact solar cells which include EWT, MWT and BJBC use in-plane interconnectors for interconnection of neighbouring cells [27]. The advantages of these cells over their conventional counterpart include: possession of reduced stress in the soldered joint, possession of minimal shadowing loss caused by metal grids, provision of more surface area for current generation, optimisation of module efficiency and improvement of aesthetics of the module [20, 28, 29].

Alternate p- and n-type silicon solar cells are bifacial screen-printed cells which use alternating p- and n-type semiconductor devices thereby allowing direct interconnection of equivalent sides on front-to-front and back-to-back of neighbouring cells [30]. The advantages of this solar cell technology compared to their conventional equivalent include

190 simpler interconnection procedure, closer assembly of cells (for aesthetic reasons) and higher  
191 yield during module fabrication.

192 Honeycomb design (HD) solar cells are cells made with surface texturing that resembles  
193 honeycomb structure. This type of design provides very effective light trapping in the cell by  
194 total internal reflection. The honeycomb texturing reduces surface reflection of the solar cells  
195 [31,32]. The interconnection of the thin HD crystalline silicon solar cells is achieved through  
196 the use of an integrated series-connection structure. The advantage of HD cell concept is that  
197 series resistance losses are reduced due to removal of areas with contact resistance which are  
198 present in conventional cells.

199 Pin up modules are back-contacted solar cells designed with a structured interconnecting  
200 back foil and limited number of holes in the wafer. The holes are used as vias and contain  
201 pins serving as interconnection from the front-side metallisation to the interconnection  
202 material at the rear [21, 33]. The advantages of Pin up modules over conventional modules  
203 include possession of minimal series resistance and shadowing losses.

204 Sliver cells are perfectly bifacial monocrystalline silicon solar cells. These cells are long,  
205 narrow, thin and symmetrical in appearance. The technology employed in the fabrication of  
206 these cells promotes economy in the usage of silicon materials. A decrease of about 10 to 20  
207 times the quantity of silicon used in other conventional technologies is obtainable when sliver  
208 cells technology is utilised [34]. The sliver cells are interconnected with two thin, narrow  
209 substrate supports to form a conventional solar cell analogue. The cells are thin with  
210 collecting junctions on both surfaces and the contacts are on the rear of the cell [35]. The  
211 advantage of sliver cells concept is that shadowing losses are minimised compared to  
212 conventional crystalline cells.

213 Spherical silicon solar cells capture light from all directions because of the spherical  
214 geometric nature of the reception surface. This design feature has the capacity to improve the  
215 amount of power the system generates to the maximum [36]. The benefits of spherical solar  
216 cells include less silicon usage, lower cost and usable in a variety of applications [37]. The  
217 spherical cells are interconnected adjacent to one another to form a mini-module in series  
218 which produces a specific constant voltage; and current which may be varied. A key  
219 advantage of spherical cells over conventional crystalline cells is that shadowing losses are  
220 effectively eliminated.

221 Silicon cells with flexible electrode wire grid (Day4 Electrode) structurally consists of  
222 transparent polymeric film, a layer of adhesive and embedded copper wires coated with low  
223 melting point alloy [38] which interconnects the cells with copper wires. The copper wires  
224 are very tiny and embedded in the transparent film. This arrangement has the advantage of  
225 minimal shadowing effect predominant in the conventional crystalline cells.

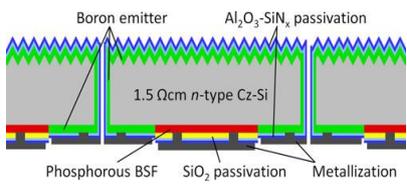
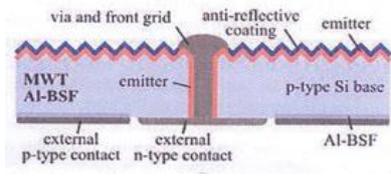
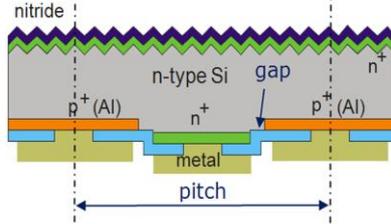
226 Although IR and laser soldering technology are used in several cell concepts, they are not the  
227 only interconnection techniques. [Techniques which include ultrasonic welding \[39\], thermal  
228 spraying \[40\] and conductive adhesives \[41\] have been successfully employed.](#) Each of these  
229 techniques induces thermo-mechanical stress in the solder joint to some degree. The

230 techniques create series resistance and shadowing losses in the solar cell. Moreover, these  
231 techniques induce thermo-mechanical stress in the interconnection joint. The mechanism of  
232 thermo-mechanical stress origin is dependent on the difference between solder melting  
233 temperature and room temperature. This conveys the concept of homologous temperature of  
234 material. Homologous temperature expresses the temperature of a material as a fraction of its  
235 melting point using the Kelvin scale. At low homologous temperatures, joint materials of  
236 interconnected solar cells are structurally modified and residual intrinsic stresses are induced  
237 in the joint. On the other hand, processing temperature for each interconnection technique is  
238 different. The typical reflow temperature for tin-silver-copper (SnAgCu) solder used for  
239 interconnection of conventional front-to-back cells is about 250 °C [42]. Similarly,  
240 processing temperature for laser spot soldering of cells is about 225 °C [26] while for  
241 ultrasonic welding, the temperature is about 177 °C [43]. Likewise, the processing  
242 temperature for interconnection of cells using thermal arc metal spraying and conductive  
243 adhesive is about 150 °C [40] and 125 °C [41] respectively.

244 Interconnection of solar cells results in bonded materials at the interconnection joint. In order  
245 to ensure that the bond has adequate strength, the bond is tested to determine its peel force.  
246 Peel force is the measure of adhesion strength required to part bonded materials. The  
247 interconnection concepts developed and their corresponding interconnection techniques with  
248 peel force and residual stress are presented in Table 1. It can be observed in the table that  
249 some interconnection concepts have more than one interconnection technique. It therefore  
250 serves as a reference guide to PV manufacturers who may be interested in making choices of  
251 technique to use when consideration on peel force and induced residual stress in the solder  
252 joint are factors.

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Table 1: Comparison of different interconnection techniques with peel force and residual stress for various interconnection concepts employed in assembly of crystalline silicon solar cells

Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Conventional front-to-back cell interconnection [24].</p> <p>Tabbing ribbon soldered to front and back of cell [25, 26].</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)
	Laser spot soldering	1-5 [46, 47]	NA
 <p>Back-contact EWT solar cells [48].</p> <p>Hole drilled for vias which allow emitter wrap through from front of the cell to the back surface [27-29, 48, 49].</p>	Laser soldering	1-5 [46,47]	NA
	Conductive adhesive	0.3-1 [50]	15-19.5 [51] (Simulation)
 <p>MWT solar cells [53].</p> <p>Similar to EWT cells but has metal grid contact on the front surface while interconnection pads for both polarities are on the rear surface [52-54].</p>	Laser soldering	1-5 [46, 47]	NA
	Conductive adhesive	0.3-1 [50]	15-19.5 [51] (Simulation)
 <p>BJ-BC solar cells [55]</p> <p>Both emitter and metallisation are located at the rear surface of the cell [55, 56]</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)

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Table 1 (Continued)

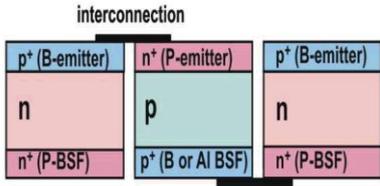
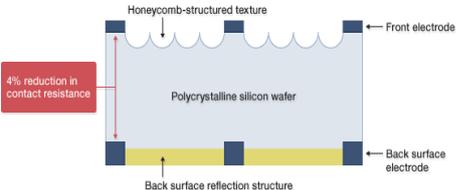
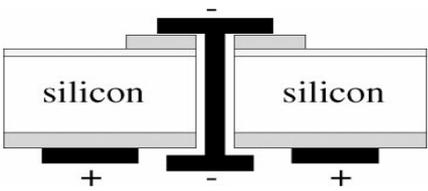
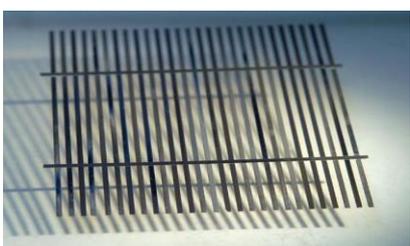
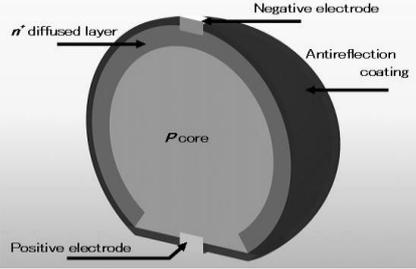
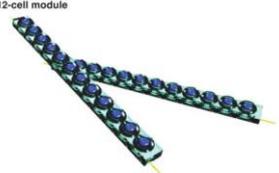
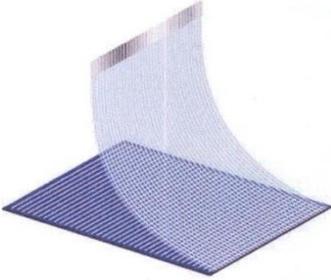
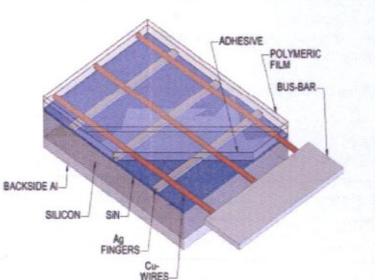
Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Alternate p- and n-type silicon solar cells [30].</p> <p>These bifacial cells allow direct interconnection of equivalent sides on front-to-front and back-to-back of neighbouring cells [30].</p>	IR soldering	2-16 [44]	49-359 [45] (Simulation)
 <p>HD solar cell [58]</p> <p>Interconnection of the thin HD cells is achieved through the use of an integrated series-connection structure [31, 32, 57, 58].</p>	IR soldering ----- Conductive adhesive	2-16 [44] ----- 0.3-1 [50]	49-359 [45] (Simulation) ----- 15-19.5 [51] (Simulation)
 <p>PUM Cell [33].</p> <p>Interconnection from the front-side metallisation to the interconnection material at the rear achieved through vias containing pins [33, 59].</p>	IR soldering ----- Thermal arc metal spraying	2-16 [44] ----- NA	49-359 [45] (Simulation) ----- NA
 <p>Sliver cells [34, 35].</p> <p>Cells interconnected by two thin, narrow substrate supports [34, 35].</p>	Solder bumps	1-5 [46, 47]	NA

Table 1 (Continued)

Interconnection concept	Inter-connection technique	Peel force (N)	Residual stress (MPa)
 <p>Spherical cell [36].</p> 	Ultrasonic welding	2-5 [62]	NA
<p>Interconnected spherical cells [37].</p> <p>Cells are interconnected adjacent to one another to form mini-modules which in turn are interconnected by ultrasonic welding [36, 37, 60, 61].</p>			
 <p>Cell with flexible electrode [64].</p> 	Conductive adhesive	0.3-1 [49]	15-19.5 [50] (Simulation)
<p>Cell in contact with electrode [65].</p> <p>Interconnection achieved using flexible Day4 electrode wire grid consisting of transparent polymeric film, a layer of adhesive and embedded copper wires coated with low melting point alloy. The wire grid is glued to the cells using adhesives to obtain interconnection [38, 63-65].</p>			

271 Furthermore, interconnection technologies for silicon solar cells are numerous and have  
272 various applications. The conventional interconnection concepts remain dominant while the  
273 other concepts are completely unconventional and modest. The review found some concepts  
274 which combine conventional with other concepts. For instance, on-laminate laser soldering  
275 (OLLS) was developed to combine the reliability potentials of conventional module assembly  
276 with the smoothness potential of the process steps in the monolithic module assembly  
277 (MMA) [66, 67]. The concept involves interconnecting solar cells on a patterned back sheet  
278 foil using conductive adhesives or low melting point solders [68].

279 Table 2 presents a comparison of interconnection technologies employed in the manufacture  
280 of silicon solar cells including thin-film silicon solar cells. The index of comparison is cell  
281 type, joint type and production status. It can be observed from the table that conventional  
282 interconnection technologies for wafer-based silicon solar cells and for thin-film silicon solar  
283 cells are the only widespread and commercially available technologies. New concepts used in  
284 solar cells interconnection are either partially available or are yet to be commercially  
285 available.

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304 Table 2: Comparison of silicon solar cells interconnection technologies in terms of cell type,  
 305 joint type and production status

	Cell type	Interconnect technology	Joint type	Production status			
				Widespread	Partially	R & D	
Silicon solar cells	Wafer-based	Conv. c-Si and mc-Si	Ribbon (front-to-back)	Solder joint	✓		
		Alternate p- and n-type	Ribbon (equivalent sides)	Solder joint		✓	
		EWT	Edge tab (back contact)	Solder/ conductive adhesive joint		✓	
		MWT	Conductive foil/Ribbon	Conductive adhesive/ Solder joint		✓	
		EWT, MWT	Bone-shaped interconnector (MMA)	Laser solder joint		✓	
		Honeycomb design	Ribbon/Adhesive	Solder/ conductive adhesive joint		✓	
		PUM	Foils with patterned conductors	Solder/thermal metal spraying		✓	
		Sliver	Substrate support bond	Solder joint		✓	
		c-Si and mc-Si	Day4 electrode	Day4 electrode adhesive joint		✓	
		Cz. Si	Spherical	Substrate support bond	Ultrasonic		
					Welded joint		✓
		Thin-film	Conv. a-Si and $\mu$ c-Si	Monolithic series	Conductive film bond		✓

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307 **3. Interconnection materials and technology reliability challenges of silicon solar cells**

308 Although it is reported in [69] that the reliability status of PV systems is good, even with a  
 309 reliable technology there is always room for improvement. With the reported recent cases of  
 310 unprecedented failure of PV modules in the tropics, the improvement of reliability of  
 311 modules has become essential more so as the improvement will encourage more system  
 312 uptake. System's reliability depends to some extent on their cost of manufacture and it is  
 313 measured by parameters which include systems performance, availability and degradation  
 314 during operation and maintenance (O&M) and predictability [70] as well. It has been widely  
 315 reported that the daily thermal cycles which PV modules are subjected to in the field is one of  
 316 the causes of degradation experienced by its interconnection. In addition to accelerating  
 317 interconnect degradation; the thermal cycling also increases series resistance [71]. As  
 318 discussed previously, silicon solar cells are interconnected with one another either by the

319 process of soldering or by the use of electrical conductive adhesive [72]. The reliability  
320 challenges of each technique are widely reported by researchers. In this section, this review  
321 will present and discuss the challenges associated with these two techniques. It will discuss  
322 the reliability of interconnection made using solder in sub-section 3.1 while in sub-section  
323 3.2, it will discuss the reliability of interconnection made using electrical conductive  
324 adhesives.

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### 327 3.1 Reliability of solder interconnection in PV modules

328 The key materials used in the assembly of conventional crystalline silicon modules include  
329 silicon, glass, copper ribbon, back sheet, encapsulant, bus-bar and solder [24]. A critical part  
330 of the module is the solder joint interconnections. They consist of many materials bonded  
331 together. The materials bonded together in the joint are the solder, bus-bar, ribbon and the  
332 silicon wafer. These materials possess different thermal and mechanical properties. In  
333 bonding, the assembly develop thermo-mechanical reliability issues which are caused by  
334 differences in the bonded materials' coefficient of thermal expansion (CTE). In PV module  
335 solder interconnection, the solder provides a connection between the electrode and ribbon.  
336 This connection is the pathway through which current flows from the silicon semiconductor  
337 to the ribbon. The PV module temperature varies according to local weather which in turn  
338 affects the rate of solder interconnection degradation. In a lifetime prediction modelling  
339 analysis [73], Han et al reported that for the same type of Si PV modules located in various  
340 weather conditions, lifetime was shortest in a desert followed by those in the tropics.

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342 Although the use of soldering process in the assembly of solar cells in PV modules has the  
343 advantage of yielding products which possess high reliability at minimal production cost, the  
344 technology occurs at high temperature with inherent potential to produce shear stress in the  
345 silicon wafer. This occurrence which is due to the differences in CTEs of the bonded  
346 interconnect materials in the assembly [74] may result in systematic grid finger interruptions  
347 at the bus-bar edges [24, 74] and also fatigue damage. In the presence of transients associated  
348 with passing clouds and daily thermal cycling, the joints are exposed to fatigue loading which  
349 leads to metal segregation, grain boundary coarsening/cracking and increased series  
350 resistance and heating [7, 75, 76]. Some approaches have been proposed to either reduce or  
351 avoid these reliability issues which have been discussed and presented earlier in  
352 unconventional interconnection concepts.

353

354 Interconnection technologies involving the use of laser soldering for interconnecting solar  
355 cells have been developed by researchers for various concepts of PV modules. Utilising laser  
356 soldering technology for interconnection has the potential to ensure that the joints are highly  
357 reliable when compared to conventional soldering technology. This is because laser soldering  
358 induces minimal thermal and mechanical stresses in the solder joints. In an experimental  
359 investigation [77], Schmidhuber et al reported that peel force in conventional soldered tabs  
360 was in the range of 1 to 3 N while that in a laser soldered tabs is about zero. This finding  
361 supports the earlier statement that laser soldering has minimal mechanical damage in the  
362 solar cell interconnection. Therefore, the adoption and use of laser soldering technology to  
363 interconnect crystalline silicon cells need to be explored as a replacement for conventional  
364 soldering technology for improved reliability of solder interconnections in crystalline PV  
365 modules.

366

367 3.2 Reliability of electrical conductive adhesive interconnection in PV modules

368 The elevated temperature soldering of cells induces stress in the cells. In addition to the  
369 induced stress, the solder joints are also stressed and deformed during operations in the field.  
370 The deformation of the joints culminates in cell warpage, breakage and ultimately system  
371 failure at prolonged operations.

372  
373 To avoid this situation, some manufacturers use electrical conductive adhesives in place of  
374 solder for the interconnection. The electrical conductive adhesives, which are made of silver-  
375 loaded epoxy resins, are being used successfully as an alternative bonding material for solar  
376 cells interconnection [78]. The use of conductive adhesives as an alternative to solder has  
377 been shown to have minimal change on the mechanical properties of the bonded materials in  
378 the joints. Similarly, its use enhances the conductivity of the joint. As this bonding process is  
379 carried out at low temperature, it leaves minimal residual stress on the joint with advantage of  
380 minimal cell breakage [78, 79]. It is pertinent to note that conductive adhesives can be used  
381 for interconnecting both crystalline and thin film solar cells.

382  
383 Although the adoption and use of this low temperature bonding technology appear to solve  
384 the initial challenge encountered in using soldering process, there are some key reliability  
385 challenges associated with modules manufactured using the process during field operations.  
386 The adhesives undergo accelerated degradation occasioned by oxidation of the adhesive  
387 material. Moreover, the adhesive-to-metal bond, which is the interconnection joint,  
388 experience de-bonding [78, 80]. The de-bonding commences with crack initiation and  
389 propagation which enables corrosion induced system failure.

390

391 **4. Future R&D challenges and opportunities**

392

393 While several crystalline silicon module concepts have been developed to address the various  
394 challenges discussed earlier, there is no single concept that has solved all the challenges.  
395 Therefore, opportunities exist for more research and development (R&D) for further  
396 improvement of the cells design and manufacture. In this regard, R&D opportunities focussed  
397 on series resistance, shadowing and recombination losses as well as induced thermo-  
398 mechanical stress are discussed as follows.

399

400 Series resistance losses in a crystalline silicon solar cell have three main causes. The first  
401 cause is the current flow through the emitter and base of the solar cell while the second cause  
402 is the contact resistance between the metal contact and the silicon. The final cause is the  
403 resistance of the top and rear metal contacts. In addition, it is also known that thermal cycling  
404 increases series resistance. Considerable R&D is required aimed at reducing series resistance  
405 losses through the decrease in metal contact resistivity which can improve energy conversion  
406 efficiency of the cells.

407 Shadowing losses result from interconnection ribbons placed on the surface of wafer-based  
408 crystalline silicon cells. Their presence on the cell surface occupies precious space thereby  
409 preventing power generation by that cell portion. Increase in the width of interconnection  
410 ribbon cross-section increases the shadowing losses proportionally. The best situation will be  
411 to completely relocate the interconnection to the back of the cell. This desire forms the basis  
412 for back contact cell concepts. However, the fabrication challenges associated with these  
413 concepts has affected the uptake of the technology. Furthermore, the reliability of these

414 concepts is yet to be proven in long-term field exposure. Thus, the R&D opportunities for  
415 reduction of shadowing losses include simplification of fabrication processes and ensuring  
416 solar cells developed are durable and reliable.

417

418 Induced thermo-mechanical stress in PV modules is a concern that requires proper attention.  
419 Photovoltaic module interconnection consisting of solder joints, ribbon and busbar are found  
420 to be the most vulnerable part to degradation and failure. As mentioned earlier, the  
421 differences in CTE among these bonded materials and long repeated temperature cycles  
422 induce thermo-mechanical strain and stress in the joint. These factors lead to module  
423 untimely failure which becomes aggravated in poor solder bonding between ribbon and silver  
424 busbar. Concerted R&D is needed for the optimization of the parameter settings involved in  
425 manufacture of these modules to improve the reliability of PV module assembly. These  
426 parameters are the dimensions of the ribbon, busbar, backsheet and any other critical  
427 dimension identified. The application of finite element modelling in the early design stage of  
428 PV modules has the potential to predict the response of the assembly to cyclic thermo-  
429 mechanical stresses and strains. The techniques could also be used to determine the optimal  
430 parameter settings of the control factors in the module assembly. This will enable the  
431 determination of an optimal parameter setting of solder joint to improve the thermo-  
432 mechanical reliability of PV module assembly. Additionally, more R&D is required for  
433 conductive adhesives used for solar cells interconnection in order to improve their durability  
434 and reliability.

435

436

## 437 **5. Summary**

438

439 A review of contacts and interconnection technologies used to assemble crystalline silicon  
440 solar cells has been presented and discussed in this paper. The review was extended to  
441 include detailed description of the concepts and interconnection technologies employed in the  
442 manufacture of unconventional silicon solar cells.

443

444 It was found that the predominant interconnection technology used in the manufacture of  
445 wafer-based silicon solar cells involves soldering of ribbon on the surface of cell. This basic  
446 technique is shown to be none ideal because the soldering process induces thermo-  
447 mechanical stresses in the cells and joints. The review results show that the process of  
448 interconnecting ribbon on the front-to-back surface of the cells leads to significant series  
449 resistance, shadowing losses. It identifies the technology of laser soldering as one which is  
450 poised to produce high reliability interconnection joints in the module. The capacity to heat  
451 only very small area of the ribbon placed on the cell enables the laser technology to induce  
452 minimal stress on the cell and joints after soldering and consequently produces quality  
453 assembly. On the other hand, it was found that adhesive-to-metal bond experiences  
454 substantial crack initiation and propagation which enables corrosion induced system failure.  
455 More review results indicate that the concepts developed for unconventional solar cell (to  
456 address the current reliability issues in the manufacture of PV modules) are yet to attain  
457 popular uptake because of lack of track record, major changes in tooling and manufacturing  
458 facilities as well as their attendant cost.

459

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464

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